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European Technical Assessment ETA-19/0175 of 2021/08/09

I GENERAL PART

Technical Assessment Body issuing the ETA and designated according to Article 29 of the Regulation (EU) No 305/2011: ETA-Denmark A/S

Trade name of the construction product:	fischer PowerFast II screws	
Product family to which the above construction product belongs:	Screws for use in timber constructions	
Manufacturer:	fischerwerke GmbH & Co. KG Klaus-Fischer-Straße 1 D-72178 Waldachtal Germany	
Manufacturing plant:	fischerwerke	
This European Technical Assessment contains:	47 pages including 2 Annexes which form an integral part of the document	
This European Technical Assessment is issued in accordance with Regulation (EU) No 305/2011, on the basis of:	European Assessment document (EAD) no. EAD 130118-01-0603 "Screws and threaded rods for use in timber constructions"	
This version replaces:	The ETA with the same number issued on 2020-01-07	



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The document refers to the following harmonized standards and European Technical Assessments (ETA):

EN 300:2006	<i>Oriented Strand boards (OSB) – Definitions, classifications and specifications</i>
EN 312:2010	Particleboards – Specifications
EN 314-2:1997	Plywood - Bonding Quality – Requirements
EN 338:2016	Structural timber – Strength classes
EN 520:2010	Gypsum plasterboards – Definitions, requirements and test methods
EN 622-2:2006	Fibreboards – Specifications – Part 2: Requirements for hardboards
EN 622-3:2006	Fibreboards – Specifications – Part 3: Requirements for medium boards
EN 622-5:2010	Fibreboards – Specifications – Part 5: Requirements for dry process boards (MDF)
EN 826:2013	Thermal insulating products for building applications – Determination of compression behaviour
EN 1990:2013	Eurocode – Basis of structural design
EN 1993-1-1:2014	<i>Eurocode 3: Design of steel structures – Part 1-1: General rules and rules for buildings</i>
EN 1995-1-1:2014	Eurocode 5: Design of timber structures – Part 1-1: General – Common rules and rules for
	buildings
EN 1995-1-2:2011	Eurocode 5: Design of timber structures – Part 1-2: General – Structural fire design
EN 13353:2011	Soli wood panels (SWP) - Requirements
EN 13986:2015	Wood-based panels for use in construction – Characterisitcs, evaluation of conformity and marking
EN 14080:2013	Timber structures – Glued laminated timber and glued solid timber – Requirements
EN 14374:2016	Timber structures – Laminated veneer lumber (LVL) – Requirements
EN 14592:2012	Timber Structures – Dowel-type fasteners - Requirements
EN 15283-2:2009	Gypsum boards with fibrous reinforcements – Definitons, requirements and test methods –
	Part 2: Gypsum fibre boards
EN 15497:2014	Structural finger jointed solid timber – Performance requirements and minimum production requirements
EN ISO 7094:2000	Plain washers - Extra large series, product grade C
ETA-14/0354:2018	Pollmeier Furnierwerkstoffe GmbH



II SPECIFIC PART OF THE EUROPEAN TECHNICAL ASSESSMENT

1 Technical description of product

»fischer PowerFast II« screws are self-tapping screws to be used in timber structures. They shall be threaded over a part of the length or over the whole length. The screws shall be produced from carbon steel wire for nominal diameters between 3,0 mm and 6,0 mm. Where corrosion protection is required, the material or coating shall be declared in accordance with the relevant specification given in Annex A of EN 14592.

The FAFS-Clip are made of zinc die cast for »fischer PowerFast II« screws with countersunk head and a diameter of 5,0 mm.

Geometry and Material

The nominal diameter d (outer thread diameter) of the screws shall not be less than 3,0 mm and not greater than 6,0 mm.

The overall length l_s of the screws, shall not be less than 20 mm and shall not be greater than 300 mm. Dimensions see Annex A.

The ratio of inner thread diameter to outer thread diameter d_1/d ranges from 0,50 to 0,80.

The screws are threaded over a minimum length l_g of 4,0 d (i.e. $l_g \ge 4,0 \cdot d$).

The thread pitch p (distance between two adjacent thread flanks) ranges from $0,50 \cdot d$ to $0,85 \cdot d$.

No breaking shall be observed at a bending angle of $\alpha \le (45/d^{0.7} + 20)^{\circ}$.

2 Specification of the intended use in accordance with the applicable EAD

The screws are used for connections in load bearing timber structures between members, softwood and hardwood of: Solid Timber (C), Glued-Laminated Timber (GL), Cross-Laminated Timber (CLT) and Laminated Veneer Lumber (LVL), similar glued members, Wood-Based Panels or steel. »fischer PowerFast II« screws with a thread over the full length can also be used as tensile or compressive reinforcement perpendicular to the grain or as shear reinforcement. Furthermore »fischer PowerFast II«

screws with diameter of 6 mm may also be used for fixing of thermal insulation on rafters and on vertical

facades and 5 mm screws can be combined with the FAFS-Clip.

Steel plates, wood-based panels and plasterboards shall only be fixed on the side of the screw head. The minimum thickness of wood-based panels should be $1,2 \cdot d$.

The following wood-based panels can be used:

- Plywood according to EN 636 or European Technical Assessment or national provisions that apply at the installation site
- Particleboard according to EN 312 or European Technical Assessment or national provisions that apply at the installation site
- Oriented Strand Board (OSB) according to EN 300 or European Technical Assessment or national provisions that apply at the installation site
- Fibreboard according to EN 622-2, EN 622-3 and EN 622-5 or European Technical Assessment (minimum density 650 kg/m³) or national provisions that apply at the installation site
- Cement-bonded particleboard according to EN 634, European Technical Assessment or national provisions at the installation site
- Solid wood panels according to EN 13353 or European Technical Assessment or national provisions that apply at the installation site
- Wood-based panels for use in constructions according to EN 13986
- Cross-Laminated Timber (CLT) according to European Technical Assessment
- Laminated Veneer Lumber (LVL) according to EN 14374 or European Technical Assessment
- Engineered wood products according to European Technical Assessments, provided that the ETA for the product provides provisions for the use of selftapping screws and these provisions are applied



The screws shall be driven into softwood and hardwood with a maximum characteristic density of 730 kg/m³ without pre-drilling or after pre-drilling (see Table 1 and Table 2) with a diameter not larger than the inner thread diameter for the length of the threaded part and with a maximum of the smooth shank diameter for the length of the smooth shank.

Table 1: Recommended pre-drilling diameters			
Bore-hole diameter [mm]			
Softwood	Hardwood		
2,0	2,5		
2,0	2,5		
2,5	3,0		
2,5	3,0		
3,0	3,0		
4,0	4,0		
	Bore-hole d Softwood 2,0 2,5 2,5 2,5 3,0		

Recommended values without pre-drilling for the maximum penetration length of the threaded part of »fischer PowerFast II« made of carbon steel in wood-based members like ash, beech and oak or LVL according to ETA-14/0354 (e.g. Baubuche) are shown in Table 2. The FAFS-Clip can be installed with or without pre-drilling (see chapter 3.7.11), recommended borehole diameter 5 mm.

Table 2: Recommended penetration length

without pre-drilling in hardwood		
Maximum penetration		
length [mm]		
40		
45		
50		
60		
70		
70		

To fix steel parts with the head side of the screw, the boreholes must be pre-drilled with a suitable diameter.

When using screws with a countersunk, step countersunk and raised countersunk head, the upper surface of the screw head must be flush with the surface of the timber part. Countersinking deeper is not permitted and should be avoided, because of damaging the surface and reduce the durability of the construction. Countersunk head screws made of carbon steel according to Annex A1 and A2 can be used together with washers according to Annex A8. Washers according to EN ISO 7094 can be used together with washers according to Annex A8.

For the use of screws in the edge side of wood-based panels one have to pre-drill with a diameter not larger than the inner thread diameter for the length of the threaded part and with a maximum of the smooth shank diameter for the length of the smooth shank.

Pan head, step countersunk and washer head screws according to Annex A3, A4 and A5, may be used together with washers according to EN ISO 7094.

»fischer PowerFast II« screws can be driven in with standard screw drillers and with torque impact screw drivers too (e.g. fischer FSS 18V 400 BL or fischer FSS 18V 600). In combination with steel plates, torque controlled tools e.g. torque wrenches have to be used. For the use of screws in wood-based panels, like particle- and fibreboards, the screws have to be tightened carefully to ensure the characteristic load bearing capacity.

The design of the connections shall be based on the characteristic load-carrying capacities of the screws.

The design capacities shall be derived from the characteristic capacities in accordance with Eurocode 5 or an appropriate national code. The screws are intended for the use of connections subjected to static or quasi-static loadings.

The zinc-coated screws are for the use in timber structures subjected to the moisture defined by the service classes 1 and 2 according to EN 1995-1-1.

The intended use of the screws is in timber connections for which all requirements of mechanical resistance, stability and safety in use in the sense of the Basic Works Requirements 1 and 4 of Regulation 305/2011 (EU) shall be fulfilled.

The provisions made in this European Technical Assessment are based on an assumed intended working life of the screws of 50 years.

The indications given on the working life cannot be interpreted as a guarantee given by the producer or Assessment Body, but are to be regarded only as a means for choosing the right products in relation to the expected economically reasonable working life of the products.



3 Performance of the product and references to the methods used for its assessment

Characteristic	Assessment of characteristic	
3.1 Mechanical resistance and stability (BWR1)		
Characteristic yield moment Characteristic withdrawal parameter Characteristic head pull-trough parameter of screws Characteristic yield strength Insertion moment Spacing, end and edge distances Slip modulus	See section 3.7 to 3.9	
Bending angle	No breaking has been observed at a bending angle of $\alpha \leq 45^{\circ}\!/d^{0.7}\!\!+\!20^{\circ}$	
Tensile strength PowerFast II	Characteristic value $f_{tens,k}$: d= 3,0 mm 3,2 kN d= 3,5 mm 4,1 kN d= 4,0 mm 5,2 kN d= 4,5 mm 6,3 kN d= 5,0 mm 8,9 kN d= 6,0 mm 13,1 kN	
Torsional strength PowerFast II	Characteristic value $f_{tor,k}$: d= 3,0 mm 1,5 Nm d= 3,5 mm 2,0 Nm d= 4,0 mm 3,0 Nm d= 4,5 mm 4,2 Nm d= 5,0 mm 6,0 Nm d= 6,0 mm 10,0 Nm Note: Ratio of the characteristic torsional strength to the mean insertion moment: $f_{tor,k} / R_{tor,mean} \ge 1,5$	
3.2 Safety in case of fire (BWR2) Reaction to fire	The screws are made from steel classified as Performance Class A1 of the characteristic reaction to fire, in accordance with the provisions of Commission Delegated Regulation 2016/364 and EC decision 96/603/EC, amended by EC Decision 2000/605/EC.	
3.3 Safety in use (BWR4)	See aspects covered by BWR1	
3.4 Durability against corrosion The screws have been assessed as he satisfactory durability and services used in timber structures using the time described in EN 1995-1-1 and subject conditions defined by service classes		
3.5 Identification	See Annex A	
3.6 Typical and special application area	See Annex B	



3.7 Mechanical Resistance and Stability

The load-carrying capacities for the »fischer PowerFast II« screws are applicable to the woodbased materials mentioned in paragraph 1 even though the term "timber" has been used in the following. European Technical Assessments for structural members or wood-based panels must be considered if applicable.

The characteristic lateral load-carrying capacities and the characteristic axial withdrawal capacities of »fischer PowerFast II« screws should be used for designs in accordance with Eurocode 5 (EN 1995-1-1) or an appropriate valid national code.

Reductions in the cross-sectional area caused by »fischer PowerFast II« screws shall be taken into account in accordance to the Eurocode 5.

3.7.1 Lateral load-carrying capacity $f_{h,k}$

The characteristic lateral load-carrying capacity of »fischer PowerFast II« screws shall be calculated according to EN 1995-1-1. The contribution of the rope effect may be considered. For the calculation of the load-carrying capacity, the following parameters should be taken into account.

3.7.1.1 Embedment strength $f_{h,a,k}$ for use in Solid Timber (EN 338, EN 15497) and Glued-Laminated Timber (EN 14080)

The embedment strength for »fischer PowerFast II« screws in non-pre-drilled holes arranged at an angle between load and grain direction, $0^{\circ} \le \alpha \le 90^{\circ}$ can be calculated with the help of equation (1).

$$f_{h,k} = 0,082 \cdot \rho_k \cdot d^{-0,3} \tag{1}$$

The embedment strength for »fischer PowerFast II« screws in pre-drilled holes arranged at an angle between load and grain direction, $0^{\circ} \le \alpha \le 90^{\circ}$ can be calculated with the help of equation (2).

$$f_{h,\alpha,k} = 0,082 \cdot \rho_k \cdot (1 - 0,01 \cdot d)$$
(2)

Note: For the calculation according to the EN 1995-1-1 for the calculation of the effective diameter the nominal diameter d should be used.

Screws parallel to the end-grain direction are only allowed for short-time loads and can be calculated with the help of equation (3).

$$f_{h,k} = 0,0076 \cdot \rho_k^{1,24} \cdot d^{-0,3}$$
(3)

Where

- α Angle between load and the grain direction [°]
- $f_{h,k}$ Characteristic embedment strength [N/mm²]
- ρ_k Characteristic timber gross density [kg/m³]
- *d* Nominal diameter of the screw [mm]

3.7.1.2 Embedment strength $f_{h,a,k}$ for use in Cross-Laminated Timber

If there are no other technical specification (ETA or hEN) for Cross-Laminated Timber (CLT), the embedment strength for screws can be calculated as following. The following specifications are only for screws with a diameter of at least 5 mm, otherwise possible influences of gaps between the single lamellas have to be considered.

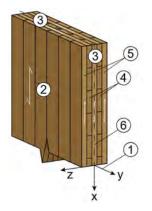


Figure 1: Notations CLT-elements

- (1) Element plane
- (2) Plane surface
- (3) Edge surface (Narrow side)
- (4) Inner layer (Inner lamellas)
- (5) Outer layer (Outer lamellas)
- (6) Middle layer (Middle lamella)

Screws in the plane surface

The embedment strength for screws in the plane surface of CLT-elements should be assumed as for solid timber according to equation (1) or (2), based on the characteristic density of the outer layer. If relevant, the angle between force and grain direction of the outer layer should be considered.

Screws in the narrow (edge) side

The embedment strength for screws in the narrow side of CLT-elements should be assumed according to equation (4).

$$f_{h,k} = 20 \cdot d^{-0.5} \tag{4}$$



3.7.1.3 Embedment strength $f_{h,\alpha,k}$ for use in Laminated Veneer Lumber according to (ETA-14/0354)

The embedment strength for »fischer PowerFast II« screws with $d \ge 5$ mm arranged at an angle between load and grain direction, $0^{\circ} \le \alpha \le 90^{\circ}$ can be calculated with the help of equation (5) in direction 90|90 (see figure 2).

$$f_{h,\alpha,k} = \frac{f_{h,0,k}}{(0,9+0,037 \cdot d) \cdot \sin^2 \alpha + \cos^2 \alpha}$$
(5)

With

3.7.1.4 Embedment strength $f_{h,\alpha,k}$ for the use in Wood-Based Panels and Plasterboards

The embedment strength for »fischer PowerFast II« screws in non-pre-drilled holes, if no other descriptions are given in Table 3, arranged at an angle α =90° to the plane surface can be calculated with equation (6).

$$f_{h,k} = f_{h,90|90,k} \tag{6}$$

Where

d

t

Nominal diameter of the screw [mm] Minimum value of the thickness of the wood-based panels/plasterboards or effective penetration depth of the screw [mm]

With

 $f_{h,90|90,k}$

Characteristic value of the embedment strength according to Table 3 and Figure 3; the influence of load-grain direction is negligible N/mm²] Table 3: Characteristic values of the embedment strength
of »fischer PowerFast II« screws in the plane surfaceMaterial $[N/mm^2]$ OSB
t > 5 mm
(EN 300) $f_{h,90/90,k} = 48 \cdot d^{-0.7} \cdot t^{-0.1}$ EGGER OSB 4 TOP,
pre-drilled
t > 10 mm
(EN 13986) $f_{h,90/90,k} = 50 \cdot d^{-0.6} \cdot t^{0.2}$ EGGER OSB 4 TOP,
without pre-drilling
t > 10 mm
(EN 13986) $f_{h,90/90,k} = 50 \cdot d^{-0.6} \cdot t^{0.2}$

pre-drilled t > 10 mm (EN 13986)	$f_{h, 90/90, k} =$	$50 \cdot d^{-0,6} \cdot t^{0,2}$
EGGER OSB 4 TOP,		
without pre-drilling		<5 ±07 01
t >10 mm	$f_{h, 90/90, k} =$	$65 \cdot d^{-0,7} \cdot t^{0,1}$
(EN 13986)		
Plywood		
t > 4 mm	$f_{h,90/90,k} =$	$65 \cdot d^{-0,7} \cdot t^{0,1}$
(EN 314-2)		
Fibreboards,		
hardboards (HDF)	f	$30 \cdot d^{-0,3} \cdot t^{0,6}$
t > 3 mm	$f_{h, 90/90, k} =$	<i>J0 u i</i>
(EN 622-2)		
Fibreboards		
medium boards		
(MDF)	$f_{h, 90/90, k} =$	$28 \cdot d^{-0,6} \cdot t^{0,6}$
t > 3 mm		
(EN 622-3)		
Particleboards		a 0 106 02
t > 5 mm	$f_{h,90/90,k} =$	$50 \cdot d^{-0,6} \cdot t^{0,2}$
(EN 312)		
Gypsum		
plasterboards	$f_{h, 90/90, k} =$	$3,9 \cdot d^{-0,6} \cdot t^{0,7}$
$t \ge 9 \text{ mm}$	J 11, 90/90, K	- ,
(EN 520)		
Gypsum boards with		
fibrous reinforcement	$f_{h, 90/90, k} =$	$7, 8 \cdot d^{-0,2} \cdot t^{0,7}$
$t \ge 9 \text{ mm}$	J 11, 20/20,1	.,
(EN 15283-2)		

The embedment strength for »fischer PowerFast II« screws in pre-drilled holes, if no other descriptions are given in Table 4, arranged at an angle $\alpha = 90^{\circ}$ to the edge surface (see Figure 4) in EGGER OSB 4 TOP can be calculated with equation (7).

$$f_{h,k} = f_{h,90|00,k} \tag{7}$$

Where

d	Nominal diameter of the screw [mm]
t	Penetration depth of the screws parallel
	to the plane surface in EGGER OSB
	TOP 4 panels [mm]
With	

fh,90 00,k	Characteristic value of the embedment
	strength; the influence of load-grain
	direction is negligible see table 4 and
	figure [N/mm ²]

Table 4: Characteristic values of the embedment strength



Material		[N/mm ²]
EGGER OSB 4 TOP, pre-drilled t >10 mm Load parallel to plane (EN 13986)	f _{h,90/00,k} =	$12 \cdot d^{-0,6} \cdot t^{0,2}$
EGGER OSB 4 TOP, without pre-drilling t >10 mm Load parallel to plane (EN 13986)	$f_{h, 90/00, k} =$	16·d ^{-0,7} ·t ^{0,1}
EGGER OSB 4 TOP, pre-drilled t >10 mm Load normal to plane (EN 13986)	$f_{h, 90/00, k} =$	$40 \cdot d^{-0,6} \cdot t^{0,2}$
EGGER OSB 4 TOP, without pre-drilling t >10 mm Load normal to plane (EN 13986)	fh,90/00,k =	$52 \cdot d^{-0,7} \cdot t^{0,1}$

of »fischer PowerFast II« screws in the edge surface

3.7.1.5 Effective number of screws per row *n*_{ef}

For laterally loaded screws, the rules for multiple fastener connections in EN 1995-1-1 should be applied.

3.7.2 Yield strength $f_{y,k}$

The characteristic yield strength of the different screw types of »fischer PowerFast II« can be taken into account as shown below.

$$f_{v,k} = 1050 \text{ N/mm}^2$$
 (8)

3.7.3 Yield moment M_{y,Rk}

The characteristic yield moment shall be calculated with the help of equation (9)

$$M_{y,Rk} = 0.15 \cdot 600 \cdot d^{2.65} \tag{9}$$

Where

 $M_{y,Rk}$ Characteristic yield moment [Nmm]dNominal diameter of the threaded part [mm]

3.7.4 Axial withdrawal capacity $f_{ax,k}$

The axial withdrawal capacity is limited by the head pull-through capacity, the withdrawal capacity and the tensile or compressive capacity of the screw. For »fischer PowerFast II« fully threaded screws, the withdrawal capacity of the thread in the member with the head may be considered instead of the head pull-through capacity.

3.7.4.1 Withdrawal capacity *F*_{ax,α,Rk} for use in Solid Timber (EN 338, EN 15497), Glued-Laminated Timber (EN 14080) and Laminated Veneer Lumber according to (ETA-14/0354)

In solid timber and glued-laminated timber of softwood, the characteristic withdrawal capacity of »fischer PowerFast II« screws, with an angle of $0^{\circ} \le \alpha \le 90^{\circ}$; shall be calculated according to equation (10).

$$F_{ax,\alpha,Rk} = n_{ef} \cdot k_{ax} \cdot f_{ax,90,k} \cdot d \cdot l_{ef} \cdot \left(\frac{\rho_k}{350}\right)^{0.8}$$
(10)

With

$$k_{ax} = \min \begin{cases} 0, 3 + (0, 7 \cdot \alpha) / 45^{\circ} \\ 1,00 \end{cases}$$
(11)

According to equation (12) the point side penetration length has to be considered between the following ranges.

$$l_{ef} = \min \begin{cases} \frac{4 \cdot d}{\sin \alpha} \\ 20 \cdot d \end{cases}$$
(12)

Where

d Outer thread diameter [mm]

 l_{ef} Penetration length of the threaded part according to EN 1995-1-1; For fully threaded screws the thread length including the head length in [mm]

 α Angle between grain and screw axis [°]

 ρ_k Characteristic timber gross density [kg/m³]

$$F_{ax,\alpha,Rk}$$
 Characteristic withdrawal capacity of the screw with an angle α to the grain [N]

$$n_{ef}$$
 Effective number of screws according to
EN 1995-1-1

With

 $f_{ax,90,k}$ Characteristic withdrawal parameter, shown in Table 5



Table 5: Characteristic withdrawal parameters			
PowerFast II	Solid Timber or		
	Glued-Laminated Timber		
d= 3,0 mm	$f_{ax,90,k} =$	15,5 N/mm ²	
d= 3,5 mm	$f_{ax,90,k} =$	14,9 N/mm ²	
d= 4,0 mm	$f_{ax,90,k} =$	14,5 N/mm ²	
d= 4,5 mm	$f_{ax,90,k} =$	14,1 N/mm ²	
d= 5,0 mm	$f_{ax,90,k} =$	13,8 N/mm ²	
d= 6,0 mm	$f_{ax,90,k} =$	12,9 N/mm ²	
PowerFast II			
	ETA-14/035	4	
d= 5,0 mm	$f_{ax,90 90,k} =$	40,0 N/mm ²	
	$f_{ax,90 00,k} =$	32,0 N/mm ²	
	$f_{ax,00 00,k} =$	32,0 N/mm ²	
d= 6,0 mm	$f_{ax,90 90,k} =$	32,0 N/mm ²	
	$f_{ax,90 00,k} =$	24,0 N/mm ²	
	$f_{ax,00 00,k} =$	24,0 N/mm ²	
$\alpha = 90 00$			
		$\alpha = 90 90$	

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Figure 2: PowerFast II in hardwood LVL

The characteristic withdrawal capacity in hardwood LVL according to ETA-14/0354 of »fischer PowerFast II« screws with an angle of $0^{\circ} \le \alpha \le 90^{\circ}$ shall be calculated according to equation (13).

$$F_{ax,\alpha,Rk} = n_{ef} \cdot k_{ax} \cdot f_{ax,\alpha|\alpha,k} \cdot d \cdot l_{ef} \cdot \left(\frac{\rho_k}{730}\right)^{0,8}$$
(13)

3.7.4.2 Withdrawal capacity *F*_{ax,Rk} for use in Cross-Laminated Timber

If there are no other technical specification (ETA or hEN) for Cross-Laminated Timber (CLT), the withdrawal capacity for screws can be calculated as following.

Screws in the plane surface

The withdrawal capacity for screws with $d \ge 6$ mm in the plane surface of CLT-elements should be assumed as for solid timber according to equation (10) based on a characteristic density of equation (14), if there are no other specifications are given. For not edge-bonded lamellas, equation (10) is only valid for screws with an outer diameter of $d \ge 5,0$ mm. If necessary gaps between the single lamellas have to be considered.

$$\rho_k = 1, 1 \cdot \rho_{lay,k} \tag{14}$$

With

 $\rho_{\text{lay},k}$ Lowest characteristic density of the lamellas in a layer of the CLT-element [kg/m³]

Screws in the narrow side

The withdrawal capacity for screws in the narrow side of CLT-elements should be assumed according to equation (15).

$$F_{ax,Rk} = 20 \cdot d^{0,8} \cdot l_{ef}^{0,9} \tag{15}$$

Screws in the narrow side should be driven perpendicular into the grain of the lamella. The penetration length has to be at least $3 \cdot d + l_{ef}$.

If it is guaranteed that the angle between the lamellas and the screw axis is $\geq 30^{\circ}$ the characteristic withdrawal capacity from equation (15) can be increased of about 25 %.

For screws penetrating more than one layer of Cross-Laminated Timber, the different layers may be considered proportionally.

3.7.4.3 Withdrawal capacity *F*_{ax,Rk} for use in Wood-Based Panels

Screws in the plane surface

The characteristic axial withdrawal capacity of »fischer PowerFast II« screws with an angle of $\alpha = 90|90$ in wood-based panels with a minimum thickness and/or a penetration depth of the threaded part of at least $4 \cdot d$ can be calculated according to equation (16) for applications in the plane surface.

$$F_{ax,\alpha,Rk} = n_{ef} \cdot f_{ax,90|90,k} \cdot d \cdot l_{ef}$$
(16)



Figure 3: PowerFast II in the plane surface

Where

 $f_{ax,90|90,k}$ Characteristic withdrawal parameter in the plane surface, shown in Table 6



»fischer PowerFast II« screws in the plane surface				
PowerFast II	OSB (EN	300)		
d= 3,0 mm	$f_{ax,90 90,k} =$	9,3 N/mm ²		
d= 3,5 mm	$f_{ax,90 90,k} =$	9,0 N/mm ²		
d= 4,0 mm	$f_{ax,90 90,k} =$	8,6 N/mm ²		
d= 4,5 mm	$f_{ax,90 90,k} =$	8,3 N/mm ²		
d= 5,0 mm	$f_{ax,90 90,k} =$	8,0 N/mm ²		
d= 6,0 mm	$f_{ax,90 90,k} =$	7,1 N/mm ²		
PowerFast II	Particleboa	rd (EN 312)		
d= 3,0 mm	$f_{ax,90 90,k} =$	11,9 N/mm ²		
d= 3,5 mm	$f_{ax,90 90,k} =$	11,1 N/mm ²		
d= 4,0 mm	$f_{ax,90 90,k} =$	10,3 N/mm ²		
d= 4,5 mm	$f_{ax,90 90,k} =$	9,5 N/mm ²		
d= 5,0 mm	$f_{ax,90 90,k} =$	8,7 N/mm ²		
d= 6,0 mm	$f_{ax,90 90,k} =$	7,1 N/mm ²		
PowerFast II	Fibreboard	S		
	(EN 622-2,	EN 622-3)		
d= 3,0 mm	$f_{ax,90 90,k} =$	13,2 N/mm ²		
d= 3,5 mm	$f_{ax,90 90,k} =$	12,4 N/mm ²		
d= 4,0 mm	$f_{ax,90 90,k} =$	11,6 N/mm ²		
d= 4,5 mm	$f_{ax,90 90,k} =$	10,8 N/mm ²		
d= 5,0 mm	$f_{ax,90 90,k} =$	10,0 N/mm ²		
d= 6,0 mm	$f_{ax,90 90,k} =$	8,5 N/mm ²		
PowerFast II	LVL (EN 1			
	$\rho_k \ge 480 \text{ kg}$	g/m ³		
d= 3,0 mm	$f_{ax,90 90,k} =$	16,0 N/mm ²		
d= 3,5 mm	$f_{ax,90 90,k} =$	15,4 N/mm ²		
d= 4,0 mm	$f_{ax,90 90,k} =$	14,7 N/mm ²		
d= 4,5 mm	$f_{ax,90 90,k} =$	14,0 N/mm ²		
d= 5,0 mm	$f_{ax,90 90,k} =$	13,3 N/mm ²		
d= 6,0 mm	$f_{ax,90 90,k} =$	12,0 N/mm ²		

Table 6: Characteristic withdrawal parameters of »fischer PowerFast II« screws in the plane surface

Screws in the narrow side

 $\alpha = 90|00$

The characteristic axial withdrawal capacity of »fischer PowerFast II« screws for pre-drilled applications in the edge surface with an angle $\alpha = 90|00$ in wood-based panels with a thickness of at least $5 \cdot d$ arranged in the center of the thickness of the panel with a penetration depth of the threaded part of the screws of at least $6 \cdot d$ can be calculated according to equation (17).

$$F_{ax,\alpha,Rk} = n_{ef} \cdot f_{ax,90|00,k} \cdot d \cdot l_{ef}$$
(17)



Where

 $f_{ax,90|00,k}$ Characteristic withdrawal parameter in the edge surface, shown in Table 7

Table 7: Characteristic withdrawal parameters of wfischer PowerFact II// screws in the adva surface

»fischer PowerFast II« screws in the edge surface					
PowerFast II	OSB (EN 3				
d= 4,0 mm	$f_{ax,90 00,k} =$	6,0 N/mm ²			
d= 4,5 mm	$f_{ax,90 00,k} =$	5,8 N/mm ²			
d= 5,0 mm	$f_{ax,90 00,k} =$	5,6 N/mm ²			
d= 6,0 mm	$f_{ax,90 00,k} =$	5,1 N/mm ²			
PowerFast II	Particleboard				
d= 4,0 mm	$f_{ax,90 00,k} =$	5,6 N/mm ²			
d= 4,5 mm	$f_{ax,90 00,k} =$	5,4 N/mm ²			
d= 5,0 mm	$f_{ax,90 00,k} =$	5,2 N/mm ²			
d= 6,0 mm	$f_{ax,90 00,k} =$	4,7 N/mm ²			
PowerFast II	Fibreboards				
	(EN 622-2, E	EN 622-3)			
d= 4,0 mm	$f_{ax,90 00,k} =$	7,0 N/mm ²			
d= 4,5 mm	$f_{ax,90 00,k} =$	6,5 N/mm ²			
d= 5,0 mm	$f_{ax,90 00,k} =$	6,0 N/mm ²			
d= 6,0 mm	$f_{ax,90 00,k} =$	5,1 N/mm ²			
PowerFast II					
	$\rho_k \ge 480 \text{ kg/s}$	m ³			
d= 4,0 mm	$f_{ax,90 00,k} =$	9,2 N/mm ²			
d= 4,5 mm	$f_{ax,90 00,k} =$	8,8 N/mm ²			
d= 5,0 mm	$f_{ax,90 00,k} =$	8,4 N/mm ²			
d= 6,0 mm	$f_{ax,90 00,k} =$	7,5 N/mm ²			

3.7.4.4 Effective number of screws *n*_{ef}

For axially loaded screws in tension, where the external force is parallel to the screw axis, the rules in EN 1995-1-1, 8.7.2 (8) should be applied.

$$n_{ef} = n^{0.9}$$
 (18)

For inclined screws in timber-to-timber or steel-totimber shear connections, where the screws are arranged under an angle $30^{\circ} \le \alpha \le 60^{\circ}$ between the shear plane and the screw axis, the effective number of screws n_{ef} should be determined with the equation below.

$$n_{ef} = \max \begin{cases} n^{0.9} \\ 0.9 \cdot n \end{cases}$$
(19)

With

n Number of (inclined/cross pairs) screws in a row parallel to the grain direction

For screws as compression reinforcement or inclined screws as fasteners in mechanically jointed beams or columns $n_{ef} = n$.



3.7.5 Head pull-through capacity fhead,k

3.7.5.1 Head pull-through capacity *f_{head,k}* for use in Solid Timber (EN 338, EN 15497), Glued-Laminated Timber (EN 14080) and Laminated Veneer Lumber according to (ETA-14/0354)

The characteristic head pull-through capacity of »fischer PowerFast II« screws in solid timber can be calculate as following.

$$F_{head,Rk} = n_{ef} \cdot f_{head,k} \cdot d_h^2 \cdot \left(\frac{\rho_k}{350}\right)^{0.8}$$
(20)

For timber elements with a thickness of at least 20 mm, the characteristic value of the head pull-through parameter $f_{head,k}$ can be taken into account as following.

Table 8: Head pull-through capacities in	n
Solid Timber, GLT, CLT and LVL	

Countersunk an	Countersunk and Raised Countersunk,				
see Annex A1 a	and A2				
d= 3,0 mm	$d_{h} = 6,0 \text{ mm}$	fhead,k=19,0 N/mm ²			
d= 3,5 mm	d _h = 7,0 mm	fhead,k=16,3 N/mm ²			
d= 4,0 mm	d _h = 8,0 mm	fhead,k=15,0 N/mm ²			
d= 4,5 mm	d _h = 8,8 mm	fhead,k=14,2 N/mm ²			
d= 5,0 mm	d _h = 9,8 mm	$f_{head,k}$ =13,4 N/mm ²			
d= 6,0 mm	d _h =11,8mm	$f_{head,k}$ =13,0 N/mm ²			
Washer head, se	ee Annex A4				
d= 5,0 mm	d _h =11,0mm	$f_{head,k} = 20,0 \text{ N/mm}^2$			
d= 6,0 mm	d _h =13,5mm	$f_{head,k}$ = 15,5 N/mm ²			
Step Countersu	nk head, see Ar	nnex A5			
d= 5,0 mm	d _h =11,0mm	$f_{head,k}$ = 19,5 N/mm ²			
d= 6,0 mm	d _h =13,5mm	$f_{head,k} = 15,0 \text{ N/mm}^2$			
Screw with clamping effect, see Annex A6					
d= 3,5 mm	d= 7,0 mm	$f_{head,k} \cdot d_h^2 = 1220 \text{ N}$			
d= 4,0 mm	d= 8,0 mm	$f_{head,k} \cdot d_h^2 = 1485 \text{ N}$			
d= 4,5 mm	d= 9,0 mm	$f_{head,k} \cdot d_h^2 = 1750 \text{ N}$			

3.7.5.2 Head pull-through capacity *f*_{head,k} for use in Wood-Based Panels

For the following wood-based panels described in Chapter 1 with a thickness of more than 20 mm the head pull-through parameter can constitute with

$$f_{head,k} = 10 \text{ N/mm}^2$$
 (21)

For wood-based panels with a thickness between 12 mm and 20 mm the characteristic value of the head pull-through parameter can be calculated with

$$f_{head,k} = 8 \text{ N/mm}^2$$
 (22)

For wood-based panels with a thickness of less than 12 mm the characteristic head pull-through capacity

shall be calculated with $f_{head,k}=8 N/mm^2$ with a limit of 400 N complying with a minimum thickness of the wood based panels of 1,2 ·d. In addition, to apply the minimum thickness of *Table 9*.

Table 9: Minimum thickness of Wood-Based Panels
be fixed on the side of the screw head

be falled on the state of the sel en head				
Wood-based panel	Min. thickness			
1	[mm]			
Plywood	6			
Oriented Strand board OSB	8			
Solid wood panels	12			
Particleboards	8			
Cement bonded particle boards	8			
Fibreboards (hard boards and	6			
medium boards)	0			
Gypsum fibre and Plasterboards	12			

3.7.5.3 Head pull/push-through capacity of the FAFS-Clip of adjustable frame screw

The characteristic head pull-through capacity in softwood of the FAFS–Clip of adjustable frame screw can be calculated for tension loads onto the screws with

$$F_{FAFS,t,Rk} = 2200 \text{ N}$$
 (23)

and for compression loads (push-through capacity) onto the screws with

$$F_{FAFS,c,Rk} = 1290 \text{ N}$$

3.7.6 Tensile capacity *f*_{tens,k}

The characteristic tensile capacity $f_{tens,k}$ of »fischer PowerFast II« screws depending on the outer diameter is given below.

Table 10: Tensile capacity					
PowerFast II					
d= 3,0 mm	$f_{tens,k} =$	3,2 kN			
d= 3,5 mm	$f_{tens,k} =$	4,1 kN			
d= 4,0 mm	$f_{tens,k} =$	5,2 kN			
d= 4,5 mm	$f_{tens,k} =$	6,3 kN			
d= 5,0 mm	$f_{tens,k} =$	8,9 kN			
d= 6,0 mm	$f_{tens,k} =$	13,1 kN			

The tear-off capacity of the screw head is greater than the tensile capacity of the screw.

3.7.7 Compression capacity

The design compressive capacity $F_{ax,Rd}$ of »fischer PowerFast II« screws with full thread along the length embedded in timber shall be calculated as following.



$$F_{ax,Rd} = \min \begin{cases} F_{ax,Rd} \\ F_{ki,Rd} \end{cases}$$
(25)

Where

 $F_{ax,Rd}$ According to equation (10) $F_{ki,Rd}$ According to equation (26)

$$F_{ki,Rd} = \kappa_c \cdot N_{pl,d} \tag{26}$$

With

$$\kappa_c = 1 \quad \text{for } \lambda \le 0, 2$$

 $\kappa_c = \frac{1}{k + \sqrt{k^2 - \overline{\lambda}^2}} \quad \text{for } \overline{\lambda} > 0, 2$
(27)

and

$$k = 0, 5 \cdot \left[1 + 0, 49 \cdot \left(\overline{\lambda} - 0, 2 \right) + \overline{\lambda}^2 \right]$$
 (28)

The relative slenderness ratio shall be calculated with

$$\overline{\lambda} = \sqrt{\frac{N_{pl,k}}{N_{ki,k}}}$$
(29)

With the characteristic value for the axial capacity in case of plastic analysis referred to the outer thread diameter. Yield strength $f_{y,k}$ see equation (8)..

$$N_{pl,k} = \frac{(0,7 \cdot d)^2 \cdot \pi}{4} \cdot f_{y,k}$$
(30)

And the characteristic ideal elastic buckling load

$$N_{ki,k} = \sqrt{c_h \cdot E_s \cdot I_s} \tag{31}$$

With the

Elastic foundation of the screw:

$$c_h = (0,19+0,0084 \cdot d) \cdot \rho_k \cdot \left(\frac{\alpha}{180^\circ} + 0,5\right)$$
 (32)

Modulus of elasticity:

$$E_s = 210.000 \text{ N/mm}^2$$
 (33)

Second moment of area:

$$I_{s} = \frac{\pi \cdot (0, 7 \cdot d)^{4}}{64}$$
(34)

Note: The compressive capacity must be modified for $f_{ax,d}$ with the factors k_{mod} and γ_M for timber according

to EN 1995-1-1 while $N_{pl,d}$ the partial-factor $\gamma_{M,1}$ for steel buckling according to EN 1993-1-1 and/or national standards respectively have to be considered.

3.7.8 Combined laterally and axially loaded screws

For connections subjected to a combination of axial and lateral loads, the following expression has to be considered according to equation (35).

$$\left(\frac{F_{ax,Ed}}{F_{ax,Rd}}\right)^2 + \left(\frac{F_{v,Ed}}{F_{v,Rd}}\right)^2 \le 1$$
(35)

With

 $F_{ax,Ed}$ Axial design action [N]

 $F_{v,Ed}$ Lateral design action [N]

- $F_{ax,Rd}$ Design load-carrying capacity of an axially loaded screw [N]
- $F_{v,Rd}$ Design load-carrying capacity of a laterally loaded screw [N]

3.7.9 Slip modulus in the serviceability limit state

Laterally loaded screws

For laterally loaded »fischer PowerFast II« screws, the slip modulus, pre-drilled or non-pre-drilled, for the serviceability limit state (SLS) should be calculated according to EN 1995-1-1 independent of the load grain-direction angle α with equation (36).

$$K_{v,ser} = k_{st} \cdot k_{sp} \cdot C_{v,ser} \tag{36}$$

With

$$k_{st} = \begin{cases} 1 & \text{for timber-timber connections} \\ 2 & \text{for steel-timber connections} \end{cases}$$

 k_{sp} Number of shear planes

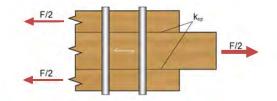


Figure 5: Definition of the shear plane k_{sp}

Where

 ρ_m Mean timber density [kg/m³]

With

 $C_{v,ser}$ Slip modulus in SLS, Table 11[N/mm]



Material $C_{v,ser}$ [N/mm]Solid Timber Glued-Laminated Timber Softwood and Hardwood (EN 338, EN 15497, EN 14080) $\rho_m^{-1.5} \cdot d$ 23(EN 338, EN 15497, EN 14080) $\rho_m^{-1.5} \cdot d$ Softwood and Hardwood (EN 300) $\delta, 8 \cdot \rho_m \cdot d^{-0.4}$ (EN 300) $V > 5 mm$ (EN 300) $\delta, 8 \cdot \rho_m \cdot d^{-0.4}$ (EN 300)Plywood t > 4 mm (EN 314-2) 740 Fibreboards t > 3 mm (EN 622-2, EN 622-3) $9 \cdot \rho_m \cdot d^{-0.9}$ Gypsum plasterboards t > 5 mm (EN 312) $3 \cdot \rho_m \cdot d^{-0.4}$ Gypsum plasterboards t $\geq 9 mm$ (EN 520) $6700 \cdot d^{-087}$ Gypsum boards with fibrous reinforcement (EN 15283-2) $1, 4 \cdot \rho_m \cdot d^{-0.7}$ LVL Soft and Hardwood $\rho_m^{-1.5} \cdot d$	Table 11: Slip modules for laterally load	led screws
Solid Timber Glued-Laminated Timber Softwood and Hardwood (EN 338, EN 15497, EN 14080) $\rho_m^{-1.5} \cdot d$ 23OSB t > 5 mm (EN 300) $\rho_m^{-1.5} \cdot d$ 23OSB t > 5 mm (EN 300) $\rho_m^{-1.5} \cdot d$ 23Plywood t > 4 mm (EN 300) $\rho_m^{-1.5} \cdot d$ 23Plywood t > 4 mm (EN 300) $\rho_m^{-1.5} \cdot d$ 23Plywood t > 4 mm (EN 314-2) $\rho_m^{-1.5} \cdot d$ 23Fibreboards t > 3 mm (EN 622-2, EN 622-3) $\rho_m \cdot d^{-0.4}$ $\rho_m^{-1.5} \cdot d^{-0.4}$ Particleboards t > 5 mm (EN 312) $\rho_m \cdot d^{-0.4}$ $\rho_m^{-1.5} \cdot d^{-0.4}$ Gypsum plasterboards t $\geq 9 mm$ (EN 520) $\rho_m \cdot d^{-0.7}$ Gypsum boards with fibrous reinforcement (EN 15283-2) $1, 4 \cdot \rho_m \cdot d^{-0.7}$	Material	$C_{v,ser}$
Glued-Laminated Timber Softwood and Hardwood (EN 338, EN 15497, EN 14080) $\rho_m^{-1.5} \cdot d$ 23OSB (EN 338, EN 15497, EN 14080)OSB $t > 5 \text{ mm}$ (EN 300) $\delta, 8 \cdot \rho_m \cdot d^{-0.4}$ (EN 300)Plywood t > 4 mm (EN 314-2)740Fibreboards t > 3 mm (EN 622-2, EN 622-3) $9 \cdot \rho_m \cdot d^{-0.9}$ Particleboards t > 5 mm (EN 312) $3 \cdot \rho_m \cdot d^{-0.4}$ (EN 312)Gypsum plasterboards t $\geq 9 \text{ mm}$ (EN 520) $6700 \cdot d^{-0.87}$ Gypsum boards with fibrous reinforcement t $\geq 9 \text{ mm}$ (EN 15283-2) $1, 4 \cdot \rho_m \cdot d^{-0.7}$		[N/mm]
Softwood and Hardwood $\rho_m^{-n^{-n}} \cdot d$ (EN 338, EN 15497, EN 14080)OSB t > 5 mm (EN 300)00 </td <td>Solid Timber</td> <td></td>	Solid Timber	
Hardwood (EN 338, EN 15497, EN 14080)OSB $t > 5 mm$ (EN 300) $f > 5 mm$ (EN 300)Plywood $t > 4 mm$ (EN 314-2)Fibreboards $t > 3 mm$ (EN 622-2, EN 622-3)Particleboards $t > 5 mm$ (EN 312)Gypsum plasterboards $t \ge 9 mm$ (EN 520)Gypsum boards with fibrous reinforcement $t \ge 9 mm$ (EN 15283-2)LVI	Glued-Laminated Timber	$a^{1,5}$ d
Hardwood (EN 338, EN 15497, EN 14080)OSB $t > 5 mm$ (EN 300) $f > 5 mm$ (EN 300)Plywood $t > 4 mm$ (EN 314-2)Fibreboards $t > 3 mm$ (EN 622-2, EN 622-3)Particleboards $t > 5 mm$ (EN 312)Gypsum plasterboards $t \ge 9 mm$ (EN 520)Gypsum boards with fibrous reinforcement $t \ge 9 mm$ (EN 15283-2)LVI	Softwood and	$\frac{p_m \cdot a}{22}$
OSB t > 5 mm (EN 300) $6,8 \cdot \rho_m \cdot d^{-0,4}$ Plywood t > 4 mm 740 (EN 314-2) 740 Fibreboards t > 3 mm $9 \cdot \rho_m \cdot d^{-0,9}$ (EN 622-2, EN 622-3) $9 \cdot \rho_m \cdot d^{-0,9}$ Particleboards t > 5 mm (EN 312) $3 \cdot \rho_m \cdot d^{-0,4}$ Gypsum plasterboards t $\geq 9 mm$ (EN 520) $6700 \cdot d^{-087}$ Gypsum boards with fibrous reinforcement t $\geq 9 mm$ (EN 15283-2) $1, 4 \cdot \rho_m \cdot d^{-0,7}$	Hardwood	23
t > 5 mm (EN 300) $6,8 \cdot \rho_m \cdot d^{-0,4}$ Plywood t > 4 mm740(EN 314-2)740Fibreboards t > 3 mm (EN 622-2, EN 622-3) $9 \cdot \rho_m \cdot d^{-0,9}$ Particleboards t > 5 mm (EN 312) $3 \cdot \rho_m \cdot d^{-0,4}$ Gypsum plasterboards t $\geq 9 mm$ (EN 520) $6700 \cdot d^{-087}$ Gypsum boards with fibrous reinforcement t $\geq 9 mm$ (EN 15283-2) $1, 4 \cdot \rho_m \cdot d^{-0,7}$	(EN 338, EN 15497, EN 14080)	
(EN 300) $Plywood$ $t > 4 mm 740$ $(EN 314-2)$ Fibreboards $t > 3 mm 9 \cdot \rho_m \cdot d^{-0.9}$ $(EN 622-2, EN 622-3)$ Particleboards $t > 5 mm 3 \cdot \rho_m \cdot d^{-0.4}$ $(EN 312)$ Gypsum plasterboards $t \ge 9 mm 6700 \cdot d^{-0.87}$ $(EN 520)$ Gypsum boards with fibrous reinforcement $t \ge 9 mm (EN 520)$ $I, 4 \cdot \rho_m \cdot d^{-0.7}$	OSB	
(EN 300) $Plywood$ $t > 4 mm 740$ $(EN 314-2)$ Fibreboards $t > 3 mm 9 \cdot \rho_m \cdot d^{-0.9}$ $(EN 622-2, EN 622-3)$ Particleboards $t > 5 mm 3 \cdot \rho_m \cdot d^{-0.4}$ $(EN 312)$ Gypsum plasterboards $t \ge 9 mm 6700 \cdot d^{-0.87}$ $(EN 520)$ Gypsum boards with fibrous reinforcement $t \ge 9 mm (EN 520)$ $I, 4 \cdot \rho_m \cdot d^{-0.7}$	t > 5 mm	$6,8 \cdot \rho_m \cdot d^{-0,4}$
$\frac{t > 4 \text{ mm}}{(EN 314-2)} = 740$ $\frac{EN 314-2}{Fibreboards}$ $\frac{t > 3 \text{ mm}}{(EN 622-2, EN 622-3)} = 9 \cdot \rho_m \cdot d^{-0,9}$ $\frac{Particleboards}{T > 5 \text{ mm}}$ $\frac{3 \cdot \rho_m \cdot d^{-0,4}}{(EN 312)}$ $\frac{Gypsum plasterboards}{T \ge 9 \text{ mm}}$ $\frac{t \ge 9 \text{ mm}}{(EN 520)} = 6700 \cdot d^{-0.87}$ $\frac{1}{4} \cdot \rho_m \cdot d^{-0,7}}{P_m \cdot d^{-0,7}}$	(EN 300)	
(EN 314-2)Fibreboardst > 3 mm(EN 622-2, EN 622-3)Particleboardst > 5 mm $2 \cdot \rho_m \cdot d^{-0,9}$ Gypsum plasterboardst ≥ 9 mm(EN 520)Gypsum boards with fibrousreinforcementt ≥ 9 mm(EN 15283-2)	Plywood	
Fibreboards t > 3 mm (EN 622-2, EN 622-3) $9 \cdot \rho_m \cdot d^{-0,9}$ Particleboards t > 5 mm (EN 312) $3 \cdot \rho_m \cdot d^{-0,4}$ Gypsum plasterboards t ≥ 9 mm (EN 520) $6700 \cdot d^{-087}$ Gypsum boards with fibrous reinforcement t ≥ 9 mm (EN 15283-2) $1, 4 \cdot \rho_m \cdot d^{-0,7}$	t > 4 mm	740
t > 3 mm (EN 622-2, EN 622-3) $9 \cdot \rho_m \cdot d^{-0,9}$ Particleboards t > 5 mm (EN 312) $3 \cdot \rho_m \cdot d^{-0,4}$ Gypsum plasterboards 	(EN 314-2)	
(EN 622-2, EN 622-3)Particleboards $t > 5 mm$ (EN 312)Gypsum plasterboards $t \ge 9 mm$ (EN 520)Gypsum boards with fibrous reinforcement $t \ge 9 mm$ (EN 15283-2)I, $4 \cdot \rho_m \cdot d^{-0,7}$	Fibreboards	
(EN 622-2, EN 622-3)Particleboards $t > 5 mm$ (EN 312)Gypsum plasterboards $t \ge 9 mm$ (EN 520)Gypsum boards with fibrous reinforcement $t \ge 9 mm$ (EN 15283-2)I, $4 \cdot \rho_m \cdot d^{-0,7}$	t > 3 mm	$9 \cdot \rho_m \cdot d^{-0,9}$
$\frac{t > 5 \text{ mm}}{(EN 312)} \frac{3 \cdot \rho_m \cdot d^{-0.4}}{6700 \cdot d^{-0.87}}$ Gypsum plasterboards $\frac{t \ge 9 \text{ mm}}{(EN 520)} \frac{6700 \cdot d^{-0.87}}{6700 \cdot d^{-0.87}}$ Gypsum boards with fibrous reinforcement $\frac{t \ge 9 \text{ mm}}{(EN 15283-2)} I.4 \cdot \rho_m \cdot d^{-0.7}$	(EN 622-2, EN 622-3)	-
(EN 312)Gypsum plasterboards $t \ge 9 \text{ mm}$ (EN 520) $6700 \cdot d^{-0.87}$ Gypsum boards with fibrous reinforcement $t \ge 9 \text{ mm}$ (EN 15283-2) $1, 4 \cdot \rho_m \cdot d^{-0.7}$	Particleboards	
(EN 312)Gypsum plasterboards $t \ge 9 \text{ mm}$ (EN 520) $6700 \cdot d^{-087}$ Gypsum boards with fibrous reinforcement $t \ge 9 \text{ mm}$ (EN 15283-2) $1, 4 \cdot \rho_m \cdot d^{-0,7}$	t > 5 mm	$3 \cdot \rho_m \cdot d^{-0,4}$
$\begin{array}{c} t \ge 9 \text{ mm} \\ (EN 520) \end{array} & 6700 \cdot d^{-087} \\ \hline \\ Gypsum \text{ boards with fibrous} \\ reinforcement \\ t \ge 9 \text{ mm} \\ (EN 15283-2) \end{array} & 1,4 \cdot \rho_m \cdot d^{-0,7} \\ \hline \\ \\ L \text{ VI} \end{array}$	(EN 312)	
(EN 520) Gypsum boards with fibrous reinforcement $t \ge 9 \text{ mm}$ (EN 15283-2) $I, 4 \cdot \rho_m \cdot d^{-0,7}$	Gypsum plasterboards	
Gypsum boards with fibrous reinforcement $t \ge 9 \text{ mm}$ (EN 15283-2) $1, 4 \cdot \rho_m \cdot d^{-0,7}$	t≥9 mm	$6700 \cdot d^{-087}$
reinforcement $t \ge 9 \text{ mm}$ (EN 15283-2) LVL	(EN 520)	
reinforcement $t \ge 9 \text{ mm}$ (EN 15283-2) LVL	Gypsum boards with fibrous	
(EN 15283-2)	• •	1 4 - 1-0.7
IVI	t≥9 mm	$1,4\cdot\rho_m\cdot a$
$\frac{\text{LVL}}{\sum \rho_m^{1.5} \cdot d}$	(EN 15283-2)	
Soft and Handwood $\rho_m^* \cdot d$	LVL	- 1,5 -1
	Soft- and Hardwood	$\underline{\rho_m^{1,5} \cdot d}$
(EN 14374) 20	(EN 14374)	20

Axially loaded screws

For axially loaded screws the slip modulus for the serviceability limit state (SLS) can be calculated according to equation (37).

$$K_{ax,ser} = C_{ax,ser} \tag{37}$$

With

- d Outer thread diameter [mm]
- lef Penetration length of the threaded part in [mm]
- Slip modulus in SLS, Table 12 [N/mm] $C_{v,ser}$

Table 12: Slip modules for axially loaded screws,				
only plane surfaces				
Material	$C_{ax,ser}$ [N/mm]			
Softwood				
$\rho_k \ge 350 \text{ kg/m}^3$	$32 \cdot d \cdot l_{ef}$			
independend of the	JZ a lej			
angle α				
Hardwood				
$ ho_k \ge 510 \text{ kg/m}^3$	$38 \cdot d \cdot l_{ef}$			
independend of the	Jo u lej			
angle α				
OSB				
t > 5 mm	$10 \cdot d \cdot l_{ef}$			
(EN 300)				
Fibreboards				
t > 3 mm	15·d·l _{ef}			
(EN 622-2, EN 622-3)				
Particleboards				
t > 5 mm	$10 \cdot d \cdot l_{ef}$			
(EN 312)				
LVL (EN 14374)				
Soft- and Hardwood				
$ ho_k \ge 480 \text{ kg/m}^3$	$28 \cdot d \cdot l_{ef}$			
α=90 90				
see Figure 2				

T 1 10 CI 11 0

3.7.10 Slip modulus in the ultimate limit state

To consider the slip modulus K_u in the ultimate limit state (ULS) Kser has to be reduced for both directions (laterally and axially) according to EN 1995-1-1 with

$$K_u = 2/3 \cdot K_{ser} \tag{38}$$

3.7.11 Minimum timber cross section, end- and edge distances

For structural timber members, minimum spacing and distances for screws in pre-drilled holes are given in EN 1995-1-1 clause 8.3.1.2 and table 8.2 as for nails in pre-drilled holes. Here, the outer thread diameter d must be considered.

Minimum thickness for structural members is in general t = 24 mm.

The FAFS-Clips may only be used in solid timber made of softwood. For the FAFS-Clip the minimum distances to the end grain in softwood has to be 60 mm. The minimum cross section for non-predrilled applications in softwood has to be at least $30 \times 50 \text{ mm}^2$, minimum width of 50 mm. With the minimum distances $a_1 \ge 12 \cdot d$ and $a_{4,t} \ge 4 \cdot d$ with d = 5 mm (see Annex A7). Predrilling is allowed with a diameter of 5 mm.



3.7.11.1 Solid Timber (EN 338, EN 15497) and **Glued-Laminated Timber (EN 14080)**

Minimum distances and spacing for laterally loaded »fischer PowerFast II« screws in non-pre-drilled holes in members of solid timber, glued-laminated timber or similar glued products with a minimum thickness $t = 12 \cdot d$ and a minimum width of 60 mm, should be chosen with Table 14

Table 13: H	ead shapes,	see Table	14 to	Table I	17

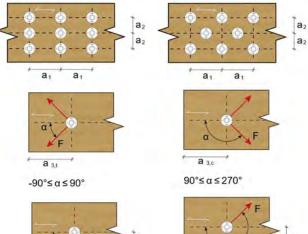
¹⁾ Head shapes	Description
Yer	Screws with countersunk, step countersunk according to Annex A1, A2 and A6
Î	Screws with pan head and washer head according to Annex A3, A4 and A5
STEEL PLATE	Screws to fix steel plates on the head side according to Annex A1, A2, A3, A4, A5

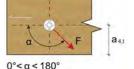
Table 14: Laterally loaded screws: Minimum end- and edge distances for solid timber and glued-laminated timber products with a maximum gross density of 480 kg/m³ for non pre-drilled screws shown in Annex A1 to A5

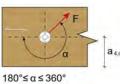
Solid Timber and Glued-Laminated Timber (EN 338, EN 15497 and EN 14080)



Head	Minii	num	spa	cing and d	listan	ces
shape ¹⁾	<i>a</i> 1	a_2	аз,с	<i>a</i> _{3,t}	<i>a</i> 4,c	<i>a</i> _{4,t}
Y	$(5+5\cdot \cos\alpha)\cdot d$	5·d	7∙d	(7+5·cosα)·d	5∙d	(5+2·sinα)·d
Î	$(5+5\cdot \cos\alpha)\cdot d$	5·d	7∙d	(5+5·cosα)·d	5∙d	(5+2·sinα)·d
STEEL	$3,5\cdot(1+ \cos\alpha)\cdot d$	3,5·d	7∙d	(5+5·cosα)·d	5·d	(5+2·sinα)·d







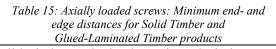
0	<α	< 1	80-

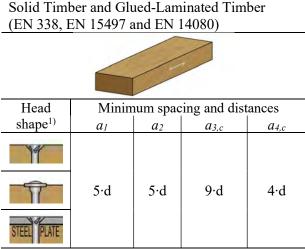
a_1 solid timber a_2 Spacing a_2 perpendicular to the grain of solid timber a_2 Distance $a_{3,c}$ from centre of the screw- grain of solid timber $a_{3,c}$ part in timber to the unloaded end grain of solid timberDistance $a_{4,c}$ from centre of the screw- a_{3,t} $a_{3,t}$ part in timber to the loaded end grain of solid timberDistance $a_{4,c}$ from centre of the screw- a_{4,c} $a_{4,c}$ part in timber to the unloaded edge of solid timber	rotations	
a_2 of solid timber Distance $a_{3,c}$ from centre of the screw- grain of solid timber $a_{3,c}$ part in timber to the unloaded end grain of solid timber Distance $a_{4,c}$ from centre of the screw- a_{3,t} part in timber to the loaded end grain of solid timber Distance $a_{4,c}$ from centre of the screw- part in timber to the unloaded edge of solid timber $a_{4,c}$ part in timber to the unloaded edge of solid timber	a_1	Spacing a_1 parallel to the grain of solid timber
$a_{3,c}$ part in timber to the unloaded end grain of solid timberDistance $a_{4,c}$ from centre of the screw- part in timber to the loaded end grain of solid timberDistance $a_{4,c}$ from centre of the screw- part in timber to the unloaded edge of solid timber $a_{4,c}$ part in timber to the unloaded edge of solid timber	<i>a</i> ₂	Spacing a_2 perpendicular to the grain of solid timber
$a_{3,t}$ part in timber to the loaded end grain of solid timberDistance $a_{4,c}$ from centre of the screw- part in timber to the unloaded edge of solid timber	<i>a</i> _{3,c}	Distance $a_{3,c}$ from centre of the screw- part in timber to the unloaded end grain of solid timber
<i>a_{4,c}</i> part in timber to the unloaded edge of solid timber	<i>a</i> _{3,t}	Distance $a_{4,c}$ from centre of the screw- part in timber to the loaded end grain of solid timber
Distance $a_{4,t}$ from centre of the screw-	<i>a</i> _{4,c}	Distance $a_{4,c}$ from centre of the screw- part in timber to the unloaded edge of solid timber
	.,.	Distance $a_{4,t}$ from centre of the screw- part in timber to the loaded edge of solid timber

¹⁾ Head shape see Table 13



Minimum distances and spacing for exclusively axially loaded »fischer PowerFast II« screws in nonpredrilled holes in members of solid timber (softwood and hardwood), glued laminated timber or similar glued products (softwood and hardwood) with a minimum thickness $t = 12 \cdot d$ and a minimum width of 60 mm, whichever is the greater, may be taken as:





¹⁾ Head shape see Table 13

Spacing a_2 perpendicular to the grain may be reduced from $5 \cdot d$ to $2, 5 \cdot d$, if the condition $a_1 \cdot a_2 \ge 25 \cdot d^2$ is fulfilled. For Douglas fir members minimum spacing and distances parallel to the grain shall be increased by 50 %.

Minimum distances from the unloaded edge perpendicular to the grain may be reduced to $3 \cdot d$ also for timber thickness $t < 5 \cdot d$, if the spacing parallel to the grain and the end distance is at least $25 \cdot d$.

3.7.11.2 Cross-Laminated Timber

Unless specified otherwise in the technical specification (ETA or hEN) of Cross-Laminated Timber, minimum distances and spacing for screws in the plane surface of Cross-Laminated timber members with a minimum thickness $t = 10 \cdot d$ may be taken as shown in Table 16 and Table 17.

Unless specified otherwise in the technical specification (ETA or hEN) of Cross-laminated timber, minimum distances and spacing for screws in the edge surface of Cross- laminated timber members with a minimum thickness $t = 10 \cdot d$ and a minimum penetration depth perpendicular to the edge surface of $10 \cdot d$ may be considered.

Table 16: Laterally and axially loaded screws:
Minimum end- and edge distances for
Cross-Laminated Timber in the plane surface

Cross-Laminated Timber

- Screws in the plane surface



I		4		1 1	• ,	
Head			-	ng and d		1
shape ¹⁾	a_1	a_2	$a_{3,c}$	<i>a</i> _{3,t}	<i>a</i> _{4,c}	<i>a</i> _{4,t}
Je	4∙d	2,5·d	6∙d	6·d	2,5·d	6∙d
T	4∙d	2,5·d	6·d	5∙d	2,5·d	6∙d
STEEL	3·d	2,0·d	6·d	5∙d	2,5·d	6·d
	, <u>a</u>	··•••••	12			a2 a2 a2
¹⁾ Head shape	saa Tab	la 13	F	a4c a4i		

¹⁾ Head shape see Table 13



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Table 17: Laterally and axially loaded screws: Minimum endand edge distances for Cross-Laminated Timber in the edge surface

Cross-Laminated Timber

- Screws in the edge surface



Head	Ν	linimur	n spacir	ng and di	stances	5
shape ¹⁾	a_1	a_2	<i>a</i> _{3,c}	<i>a</i> _{3,t}	<i>a</i> _{4,c}	$a_{4,t}$
19	10·d	3·d	7∙d	12·d	5∙d	5·d
Î	10·d	3·d	7·d	12·d	5∙d	5·d
STEEL	7·d	3·d	7·d	12·d	5·d	5·d
-, <u>a</u> ₁₂ , <u>a</u> , 	, a, -•	<u></u>	a,	a, a, a, a, a, a, a, a, a, a, a, a, b, a, a, b, a, a, b, a,		$\begin{array}{c} a_{3c} \\ a_{3c} \\ \hline \\ a_{3c} \\ \hline \\ a_{3c} \\ a_{3c}$

Notations

a_1	Spacing a_1 parallel to the plane direction of the CLT-panel
a_2	Spacing a_2 perpendicular to plane direction of the CLT-panel
<i>a</i> _{3,c}	Distance $a_{3,c}$ from centre of the screw- part in timber to the unloaded edge in plane direction of the CLT-panel
<i>a</i> _{3,t}	Distance $a_{3,t}$ from centre of the screw- part in timber to the loaded edge in plane direction of the CLT-panel
<i>a</i> _{4,c}	Distance $a_{4,c}$ from centre of the screw- part in timber to the unloaded edge perpendicular to the plane direction of the CLT-panel
<i>a</i> _{4,t}	Distance $a_{4,t}$ from centre of the screw- part in timber to the loaded edge perpendicular to the plane direction of the CLT-panel
1) 11 1 1	T 11 12

¹⁾ Head shape see Table 13

For a crossed screw couple, the minimum spacing between the crossing screws should be at least $1,5 \cdot d$.



3.8 Durability against corrosion

3.8.1 Corrosion protection in Service Class 1 and 2

The »fischer PowerFast II« screws are produced from carbon steel. They are zinc-plated (e.g. yellowbonus-zinc-coated, blue-zinced), zinced or burnished, nickel-plated or brass-plated. The mean thickness of the zinc-plated screws is min. 5 µm.

3.9 General aspects related to the intended use of the product

The screws are manufactured in accordance with the provisions of the European Technical Assessment using the automated manufacturing process as identified during the inspection of the plant by the assessment body issuing the ETA and the notified body and laid down in the technical documentation. The installation shall be carried out in accordance with Eurocode 5 or an appropriate national code and in accordance with the instructions from fischerwerke GmbH & Co. KG.



4 Attestation and verification of constancy of performance (AVCP)

4.1 AVCP system

According to the decision 97/176/EC of the European Commission, as amended, the system(s) of assessment and verification of constancy of performance (see Annex V to Regulation (EU) No 305/2011) is 3.

5 Technical details necessary for the implementation of the AVCP system, as foreseen in the applicable EAD

Technical details necessary for the implementation of the AVCP system are laid down in the control plan deposited at ETA-Danmark prior to CE-marking.

Issued in Copenhagen on 2021-08-09 by

Thomas Bruun Managing Director, ETA-Danmark



Annex A: Product details and definitions Table A1: Screw sizes and material

					ls ²⁾									
	Lindo	rhead	-		lgf									
	millin	g pockets ¹⁾	g.						,	Trad	e mark ¹⁾			
		ъ	2 mm	e fe fe		IAA	111	σŢ	•			3.		
		<u> </u>	h			lgp			Drive PZ		Dri	e ve TX		
1)		Shank ribs ¹⁾					Cor	emiller ¹⁾				_		
¹⁾ optiona Carbon												Figure	not to scal	e
 Possible 	e surface t	reatments		zinc-pla plated, l			lated, b	lue zinc	-plated ≧	≥12µn	ı, bonus-z	zinc-coa	ted, bur	rnishe
	al diame			,0		,5	4	,0	4		5	,0		6,0
	er thread o			00		50		00	4,			10		,00
	<u>w. deviatio</u> er thread di		$\pm 0,25$ $\pm 0,25$ eter 1,95 2,20					, <u>30</u> 50	±0	<u>,30</u> 75) <u>,30</u> 25		0,30 95
14	w. deviatio											23),20	3,95 ± 0,20	
Hea	ad diamete		<u>± 0,18</u> ± 0,18 6,00 7,00					± 0,20 ± 0,20 8,00 8,80				80		1,80
	w. deviatio		± 0,50 ± 0,50 ± 0,60							± 0,60 ± 0,60			± 0,60	
	ank diamet			25		60		90	3,2		_	70		,30
	w. deviation ad height	ות),15 30		± 0,15 ± 0,15 ± 0,15 ± 0,15 2,50 2,80 2,90 3,40								0,15 ,50
	Drive TX			0	10	20		20	20 20 25					, <u>00</u> 30
	Drive PZ			1		2		2	2	2		3		
Screv	Screw length l_{s^2} Standard thread length l_{gf} = Full thread l_{gp} = Pa								Partia	tial thread Tolerance: \pm 2				
lominal length	min	max	\mathbf{l}_{gf}	l _{gp}	l _{gf}	l _{gp}	l _{gf}	l _{gp}	l _{gf}	l _{gp}	l _{gf}	l _{gp}	l _{gf}	l _{gp}
20	l _s –1,05	l _s +1,05	16		16									
25	l _s –1,25	l₅ +1,25	21	18	21	18	20	18	20					
30 35	l _s –1,25 l _s –1,50	ls +1,25 ls +1,50	26 31	18 24	26 31	18 24	25 30	18 24	25 30	18 24	24 29	24	28	
40	ls -1,50	ls +1,50	36	24	36	24	35	24	35	24	34	24	33	2
45	l _s –1,50	ls +1,50	41	30	41	30	40	30	40	30	39	30	38	3
50	l _s –1,50	l _s +1,50			46	30	45	30	45	30	44	30	43	3
55	l _s –1,75						50	36	50	36	49	36	48	3
60	ls -1,75						55	36	55	36	54	36	53	3
70 80	l _s –1,75 l _s –1,75							42 45	65 75	42 45	64 74	42 45	63 73	4
90	ls -2,00											54		5
100	ls –2,00											60		6
110	ls -2,00											70		7
120	l _s –2,00 ps of 10m	ls +2,00										70		7
130-300	ls –3,00													7
		10 - 0,00	All sizes in											
⁾ Other scr lengths a	ew lengths re allowed	al thread > s with l _s mi .,l _{gp} ≤ 18mi	n ≤ l₅ ≤	l₅ max a	and othe	er thread	-			-		tandard	thread	
fischer PowerFast II Annex A1 of European Technical Assessment														

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Table A2: Screw sizes and material

PowerFast II - Self-drilling screw – Raised countersunk head with full- or partial thread													al thre	ad
		 - -			ls ²⁾									
	Underhead milling poc	t kets ¹⁾	-		lgf		-			_	Trade mark ¹⁾			
		- To							(0	\checkmark	induc induc			
		ਚ	in a a	231	L I I I	IBB		<u>6</u>]0				.)	
	Shank	ribe ¹⁾	-/	-		lgp		oremiller ¹⁾	Drive	PZ		Drive T	x	
¹⁾ optional		Jerniner				F	igure not	to scale						
CarborPossible	e surface t	reatments		zinc-pla plated, l			olated, b	lue zinc	-plated 2	≥12µn	n, bonus-z	zinc-coa	ted, bur	nishe
	al diame			,0		,5		,0		,5		,0		6,0
A	er thread one of the thread of		00),25		50),25		00 ,30		50 ,30	5,10 ± 0,30			,00),30	
Inn	er thread di		20		50		75		25		,95			
d ₁ Allo	w. deviatio	on	± C	95),18	± C),18	± 0	,20	± 0	,20	±C),20	± (0,20
d. –	ad diamete w. deviatio		6,	,	00),50	· · · · ·	00		80 ,60	-	80		1,80 0,60	
	ank diamet),50 25		60		± 0,60 2,90			± 0,60 3,70			,30
d	w. deviatio),15),15	± 0,15		3,20 ± 0,15		3,70 ± 0,15),00),15
	Head height 1,80						2,40 20		2,70		3,00			,60
	Drive TX 10 Drive PZ 1									20	20	25 2		30 3
	Drive PZ122Screw length l_s^{2} Standard thread length l_{gf} = Full thread l_{gp} =Partial 1									_		-		
Nominal length	min	max	l _{gf}	l _{gp}	l _{gf}	l _{gp}	l _{gf}	lgp	l _{gf}	l _{gp}	l _{gf}	l _{gp}	l _{gf}	l _{gp}
20	l _s –1,05	l₅ +1,05	16		16									
25	l _s –1,25	ls +1,25	21	18	21	18	20	18	20					
30 35	l _s –1,25 l _s –1,50	ls +1,25 ls +1,50	26 31	18 24	26 31	18 24	25 30	18 24	25 30	18 24	24 29	24	28	
40	$l_{s} = 1,50$ $l_{s} = 1,50$	ls +1,50	36	24	36	24	35	24	35	24	34	24	33	28
45	l _s –1,50	l _s +1,50	41	30	41	30	40	30	40	30	39	30	38	30
50	l _s –1,50	ls +1,50			46	30	45	30	45	30	44	30	43	30
55	l _s –1,75						50 55	36 36	50 55	36 36	49 54	36	48 53	36 36
60 70	ls -1,75						55	42	65	42	64	36 42	63	42
80	l _s –1,75							45	75	45	74	45	73	45
90	ls -2,00	ls +2,00										54		54
100	ls -2,00											60		60
110 120	$l_{s} = -2,00$										_	70		70 70
-	ps of 10m										1	10		10
130-300	l _s -3,00	l _s +3,00												70
130-300 Screws ²⁾ Other sc	l _s –3,00 with partia rew lengths re allowed	m l _s +3,00 al thread > s with l _s mi	n ≤ l₅ ≤	l₅ max a	and othe	er thread	-					tandard		7
	fischer PowerFast II Screw sizes and material Annex A2 of European Technical Assessment ETA-19/0175													



Table A3: Screw sizes and material

PowerFast II - Self-drilling screw - Pan head with full- or partial thread													ad		
		H	-		ls ²⁾		-								
					lgf		-								
			a							Tr	ade mark	Ν			
									()	\star		A			
		- ਦ	19-9-9-	<u>1</u>	LLL [IBA	i def	<u>a 19</u>	(•₽			(O))		
		h	_/	_		lgp \			Drive	PZ		Drive T	<		
	Shank	ribs ¹⁾					Co	oremiller ¹⁾							
 ¹⁾optional Carbon 	Staal											F	igure not	to scale	
	le surface t	reatments:			ated, blu orass pla		olated, b	lue zinc	-plated	≥12µm	, bonus-z	zinc-coa	ated, bu	rnished,	
Nomir	nal diame	eter		,0	1	,5	4	,0	4	,5	5	,0	6	6,0	
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $,00	
Allo),30 75),30 25		0,30	
	er thread di ow. deviatio			95 .18		20),18		50),20		75),20	-	25),20	3,95 ± 0,20		
He	ad diamete			00		00		00		00	-	,00		2,00	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $										_),60	± 0,60			
												,30			
Allow. deviation $\pm 0,15$ $\pm 0,15$ $\pm 0,15$ $\pm 0,15$ $\pm 0,15$ h Head height 2,30 2,50 2,80 2,80 3,40										± 0,15 3,40					
	Drive TX 10 10 20 20 20 20									25		30			
	Drive TX 10 10 20 <									2		3			
	w length l	s ²⁾	Star	dard th	read le	ength	l _{gf} = Ful	ll thread	d l _{gp} =	Partial	thread	Tolera	ance: ±	ce: ± 2,0 ³⁾	
Nominal length	min	max	\mathbf{l}_{gf}	l _{gp}	l _{gf}	l _{gp}	l _{gf}	l _{gp}	l _{gf}	l _{gp}	l _{gf}	l _{gp}	l _{gf}	l _{gp}	
20	ls -1,05	ls +1,05	16	10	16	10		10							
25 30	l _s –1,25	l₅ +1,25 l₅ +1,25	21 26	18 18	21 26	18 18	20 25	18 18	20 25	18	24				
35	l _s –1,50	l _s +1,50	31	24	31	24	30	24	30	24	29	24	28		
40	ls –1,50	ls +1,50	36	28	36	28	35	28	35	28	34	28	33	28	
45 50	ls -1,50	ls +1,50	41	30	41 46	30 30	40 45	30 30	40 45	30 30	39 44	30 30	38 43	30 30	
50	l _s –1,50	ls +1,50 ls +1,75			40	30	45 50	30	45 50	30	44	30	43	30	
60	ls -1,75	ls +1,75					55	36	55	36	54	36	53	36	
70	ls –1,75	l₅ +1,75						42	65	42	64	42	63	42	
80	l₅ –1,75	l _s +1,75						45	75	45	74	45	73	45	
90 100	l _s -2,00	ls +2,00 ls +2,00										54 60	<u> </u>	54 60	
110	l _s –2,00	l _s +2,00 l _s +2,00									1	70		70	
120	ls -2,00	ls +2,00										70		70	
	eps of 10m													70	
130-300	l _s –3,00	l _s +3,00										A 11	eizoo ir	70	
130-300 ls -3,00 ls +3,00 70 All sizes in mm • Screws with partial thread > 60 mm ls with shank ribs 2) Other screw lengths with ls min ≤ ls ≤ ls max and other thread lengths lgf resp. lgp ≥ 4xd up to max. standard thread lengths are allowed 3) For 10 mm ≤ lgf resp.,lgp ≤ 18 mm → tolerance ±1,5 mm and for 18 mm < lgf resp. lgp ≤ 30 mm → tolerance ±1,7 mm															
					erFast						o [:] Techni	Annex f Euro cal As TA-19	pean ssessi		



Table A4: Screw sizes and material

Р	owerFa	st II - Se	əlf-dri	illing	screw	/ – Wa	asher head with full-	or partial thread
¹⁾ optional	Shan	Trade mark ¹⁾						
 Carbor 		reatments			ated, blu brass pl		olated, blue zinc-plated ≥12µ	m, bonus-zinc-coated, burnished,
Nomir	al diame	eter		,0	1	,0		
	ter thread			10		,00		
Allo	ow. deviation er thread di			,30 25),30 ,95	4	
	ow. deviation			,20),20	1	
d He	ad diamete	er	11	,00	13	5,50]	
Allo	ow. deviatio			,00		1,00		
	ank diamet			70		,30		
	ow. deviation ad height			,15 00),15 ,10		
	Drive TX		20	25		30		
	Drive PZ			2		3		
Scre	w length l	.s ²⁾	Stan	dard th	nread le	ength	l _{gf} = Full thread l _{gp} =Part	ial thread Tolerance: \pm 2,0 ³⁾
Nominal	min	max	l _{gf}	lgp	l _{gf}	l _{gp}		
length			٠yı	٩p	•gi	•gp		
20 25	<u>ls -1,05</u> ls -1,25							
30	ls –1,25	ls +1,25	24					
35	ls -1,50	l _s +1,50	29	24	28			
40	ls –1,50	l _s +1,50	34	28	33	28		
45	l _s −1,50	l _s +1,50	39	30	38	30		
50 55	l _s –1,50	l _s +1,50 l _s +1,75	44 49	30 36	43 48	30 36		
60	ls -1,75	ls +1,75	54	36	53	36		
70	l _s –1,75		64	42	63	42		
80	l _s –1,75	l _s +1,75	74	45	73	45		
90	l _s –2,00			54		54	{	
100 110	l _s -2,00	l _s +2,00 l _s +2,00		60 70		60 70	1	
120		$l_{s} + 2,00$ $l_{s} + 2,00$		70		70	1	
	eps of 10m					_]	
130-300	l _s –3,00	ls +3,00				70		· · · ·
²⁾ Other sc lengths a	rew length re allowed		n ≤ l₅ ≤	l₅ max a	and othe	er threa	d lengths l _{gf} resp. l _{gp} ≥ 4xd up or 18 mm < l _{gf} resp. l _{gp} ≤ 30n	
fischer PowerFast II Annex A4 of European								
		Sc	rew si	zes ar	nd mat	erial		Technical Assessment ETA-19/0175



Table A5: Screw sizes and material

 Carbon Steel Possible surface treatments: yellow zinc-plated, blue zinc-plated, blue zinc-plated ≥12µm, bonus-zinc-coated, b nickel plated, brass plated Nominal diameter 5,0 6,0 Allow. deviation ± 0,30 ± 0,30 ± 0,30 ± 0,30 ± 0,30 ± 0,20 ± 0,15 ± 1,50 <li< th=""><th>thread</th><th>h full- or partial thre</th><th>ead wit</th><th colspan="9">PowerFast II - Self-drilling screw – Step Countersunk h</th></li<>	thread	h full- or partial thre	ead wit	PowerFast II - Self-drilling screw – Step Countersunk h										
 Carbon Steel Possible surface treatments: yellow zinc-plated, blue zinc-plated, blue zinc-plated ≥12µm, bonus-zinc-coated, b nickel plated, brass plated Nominal diameter 5,0 6,0 d Allow. deviation ± 0,30 ± 0,30 d Allow. deviation ± 0,20 ± 0,20 d Head diameter 3,70 4,30 d Head diameter 3,70 4,30 d Underhead diameter 3,70 4,30 Allow. deviation ± 0,15 ± 0,15 h Head neight 3,30 4,20 Drive FX 20 25 30 Drive FX 20 25 30 Drive FZ 2 3 Screw length Is²⁰ Standard thread length Igr = Full thread Igp =Partial thread Tolerance: Nominal min max Igr Igg Igg Igg 20 Igg Igg Igg Igg Igg 21 Igg Igg Igg Igg Igg Igg Igg Igg 30 4.1,50 4.2,00 5.4 5.4 6.0 1.4,1,50 4.2,00 5.4 7.4 7.4 7.4 7.4 7.4 7.4		Drive TX	lgf											
 Possible surface treatments: yellow zinc-plated, blue zinc-plated blue zinc-plated ≥12µm, bonus-zinc-coated, brickel plated, brass plated Nominal diameter 5,0 6,0 d Outer thread diameter 3,10 ± 0,30 ± 0,20 ± 0,00 ± 1,00 ± 1,10 ± 1,25 ± 1,25<th>ire not to scale</th><th>Figure not t</th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th>¹⁾op</th>	ire not to scale	Figure not t											¹⁾ op	
Nominal diameter5,06,0dOuter thread diameter5,106,00Allow. deviation± 0,30± 0,30d1Inner thread diameter3,253,95Allow. deviation± 0,20dnHead diameter11,00d1Underhead diameter6,407,50Allow. deviation± 1,00d2Underhead diameter3,704,30Allow. deviation± 0,15hHead height3,304,20Drive TX202530Drive PZ230Le-1,25Le-1,25Le+1,2520Le-1,25Le+1,25Le+1,2530Le-1,25Le+1,25Le+1,2530Le-1,25Le+1,50Le+1,5033Le-1,50Le+1,50Le+1,50342835Le-1,50Le+1,50Le+1,5036Le-1,50Le+1,554437Le+1,5538Le-1,50Le+1,75Le+1,7559Le-2,00Le-2,00Le+2,00546533670Le-2,00Le-2,00Le+2,0070130Le-2,00Le-2,00Le+2,0070130Le-2,00Le-2,00Le+2,0070130Le-2,00Le-2,00Le+2,007013014Le-2,00	l, burnished,	ım, bonus-zinc-coated, burn	lated ≥12µ	d, blue zinc-p					reatments:	e tr			•	
a Allow. deviation ± 0.30 ± 0.30 d1 Inner thread diameter 3,25 3,95 d1 Allow. deviation ± 0,20 ± 0,20 dh Head diameter 11,00 ± 3,50 dalow. deviation ± 1,00 ± 1,00 di. Underhead diameter -6,40 7.50 di. Shank diameter -3,70 di. Inderhead diameter -6,40 7,50 di. Shank diameter -3,70 4,30 di. Drive TX 20 25 30 Drive PZ 2 3 3 3 4,20 Drive PZ 2 3 3 3 1 3 20 ls-1,25 ls+1,25 - - 3 3 1 1 30 ls-1,25 ls+1,50 34 28 33 28 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1						1			eter	ne	al diam	Nomin		
d1Inner thread diameter3,253,95Allow. deviation± 0,20± 0,20dhHead diameter11,00± 1,00dkUnderhead diameter6,407,50dkShahk diameter3,704,30dkAllow. deviation± 0,15± 0,15hHead height3,304,20Drive PZ23Screw length L2Standard thread length Lgr = Full thread Lgp =Partial thread Tolerance:Nominalminmaxlengthminmaxlegflgrlgr20ls-1,05ls+1,2523Ls-1,25ls+1,2530ls-1,25ls+1,2530ls-1,50ls+1,5034283328ls-1,50ls+1,5039ls-1,50ls+1,5034283335ls-1,75ls+1,7544304330ls-1,75ls+1,7590ls-2,00ls+2,0070ls-2,00ls+2,0070ls-2,00ls+2,0070ls-2,00ls+2,0070ls-2,00ls+3,0070ls-2,00ls+3,0070ls-2,00ls+3,0070ls-3,00ls+3,0070ls-3,00ls+3,0070ls-3,00ls+3,0070ls-3,00ls+3,0070ls-3,00ls+3,0070ls-3,00ls+3,0070 <t< td=""><td></td><th></th><th></th><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>d</td></t<>													d	
Allow. deviation ± 0,20 ± 0,20 dh Head diameter 11,00 13,50 dh Allow. deviation ± 1,00 ± 1,00 dh Allow. deviation ± 0,15 ± 0,15 h Head height 3,30 4,20 Drive PZ 2 3 Screw length ls ² Standard thread length lgr = Full thread lgp =Partial thread Tolerance: Nominal min max lgr l					95	3,	-		ameter	dia	er thread d	Inne	4	
Ch Allow. deviation ± 1,00 ± 1,00 d _a Underhead diameter 6,40 7,50 d _b Shank diameter 3,70 4,30 d _b Shank diameter 3,70 4,30 Drive TX 20 25 30 Drive TX 20 25 30 Screw length l _a ²⁾ Standard thread length l _{gf} = Full thread l _{gp} =Partial thread Tolerance: Nominal length min max l _{gf} l _{gg} l _{gf} l _{gp} 20 l _a -1,05 l _a +1,05												_		
duUnderhead diameter6,407,50dsShank diameter3,704,30hHlow. deviation± 0,15± 0,15hHead height3,304,20Drive TX202530Drive PZ23Screw length Ls ² Standard thread length Lgr = Full thread Lgp = Partial thread Tolerance:NominalminmaxLgrLgrLgr20Ls -1,05Ls +1,05-25Ls -1,25Ls +1,25-30Ls -1,25Ls +1,25-30Ls -1,25Ls +1,503444304330Ls -1,50Ls +1,5044304330Ls -1,75Ls +1,5044304330Ls -1,75Ls +1,7544304330Ls -1,75Ls +1,7544304330Ls -2,00Ls +2,0050Ls -1,75Ls +1,75444263428040Ls -2,00Ls +2,0070L-2,00120Ls -2,00Ls +2,0070120Ls -2,00130-300Ls -3,00Ls +3,00130-300Ls -3,00Ls +3,0020Other screw lengths with Ls min ≤ Ls ≤ Ls max and other thread lengths Lgr resp. Lgp ≤ 30 mm → tolerance ±1,7 mr30Ls -2,00Ls +3,00310Screws with partial thread > 60 mm Ls with s													dh	
a_s Allow. deviation± 0,15± 0,15hHead height3,304,20Drive TX202530Drive PZ23Screw length l_s^{2} Standard thread length l_{gf} = Full thread l_{gp} =Partial thread Tolerance:Nominalminmax l_{gf} l_{gg} l_{gf} l_{gp} 20 $l_s - 1, 05$ $l_s + 1, 05$ 125 $l_s - 1, 25$ $l_s + 1, 25$ 130 $l_s - 1, 25$ $l_s + 1, 25$ 130 $l_s - 1, 25$ $l_s + 1, 25$ 130 $l_s - 1, 50$ $l_s + 1, 50$ 342845 $l_s - 1, 50$ $l_s + 1, 50$ 39303830363650 $l_s - 1, 75$ $l_s + 1, 75$ 4430 $l_s - 1, 75$ $l_s + 1, 75$ 4430 $l_s - 1, 75$ $l_s + 1, 75$ 4430 $l_s - 1, 75$ $l_s + 1, 75$ 5430 $l_s - 2, 00$ $l_s + 2, 00$ 5454 $l_0 - 1, 75$ $l_s + 1, 75$ 7445 g_1 $l_s - 2, 00$ $l_s + 2, 00$ 90 $l_s - 2, 00$ $l_s + 2, 00$ 70120 $l_s - 2, 00$ $l_s + 3, 00$ 70130-300 $l_s - 3, 00$ $l_s > l_s$ max and other thread lengths l_{gr} resp. $l_{gp} > 4xd$ up to max. standard thread lengths are alloweda) Other screw lengths with l_s min $\leq l_s < l_s$ max and other thread lengths l_{gr} resp. $l_{gp} < 30$ mm \rightarrow tole					50	7,	40	6,	ameter	dia	derhead d	Und	du	
h Head height 3,30 4,20 Drive TX 20 25 30 Drive PZ 2 3 Screw length ls ² Standard thread length lgr = Full thread lgp =Partial thread Tolerance: Nominal length min max lgr lgr lgr lgr lgr lgr = Full thread lgp =Partial thread Tolerance: Nominal length min max lgr lgr lgr lgr lgr lgr lgr lgr = Full thread lgp =Partial thread Tolerance: Nominal length min max lgr lgr lgr lgr lgr lgr = Full thread lgp =Partial thread Tolerance: Nominal length min max lgr lgr lgr lgr lgr lgr = Full thread lgp =Partial thread Tolerance: 30 ls -1,25 ls +1,55 ls -1,25 ls +1,55 ls -1,50 30 ls -1,50 ls +1,50 34 28 33 28 45 ls -1,50 ls +1,55 34 26 33 36 50 ls +1,55 14,43 30 33 36 36 60 ls -1,75 ls +1,75 54 36 53 36						· · · · · · · · · · · · · · · · · · ·							ds	
Drive PZ 2 3 Screw length ls ²) Standard thread length lgf = Full thread lgp =Partial thread Tolerance: Nominal length min max lgf lgp lgf lgp lgf lgp 20 ls -1.05 ls +1.05 -					20	4,	30		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,				h	
Screw length l _s ² Standard thread length l _{gf} = Full thread l _{gp} =Partial thread Tolerance: Nominal length min max l _{gf} l _{gf} l _{gf} l _{gf} l _{gp} 20 l _s -1,05 l _s +1,05							Drive TX 20 25							
Nominal length min max lgf lgp lgf lgp lgf lgp 20 ls -1,05 ls +1,05 - - - - - 30 ls -1,25 ls +1,25 - - - - - 30 ls -1,26 ls +1,25 - - - - - 30 ls -1,25 ls +1,25 - - - - - 30 ls -1,50 ls +1,50 29 24 28 - - 40 ls -1,50 ls +1,50 34 28 33 28 - - 45 ls -1,75 ls +1,50 44 30 43 30 - - - - 50 ls -1,75 ls +1,75 54 36 42 63 42 -	e: + 2 0 ³⁾	ial thread Tolerance: + (Im =Part	Full thread I	0		_	-	2)					
length ls ls ls ls ls 20 ls = 1,05 ls + 1,05 is is is 25 ls = 1,25 ls + 1,25 is is is is 30 ls = 1,25 ls + 1,25 is is is is is 30 ls = 1,50 ls + 1,50 29 24 28 is is 40 ls = 1,50 ls + 1,50 34 28 33 28 is 45 ls = -1,50 ls + 1,50 34 28 33 28 45 ls = -1,75 ls + 1,50 34 30 43 30 55 ls = -1,75 ls + 1,75 54 36 53 36 70 ls = -1,75 ls + 1,75 74 45 73 45 90 ls = -2,00 ls + 2,00 70 70 70 120 ls = -2,00 ls + 2,00 70 70 70 130-300 ls - 3,00 ls + 3,00 70 70 70			typ i dire									minal		
25 ls -1,25 ls +1,25 Image: start st					36	9.	96	9.	l₅ +1.05	5	ls –1.05			
35 ls -1,50 ls +1,50 29 24 28 40 ls -1,50 ls +1,50 34 28 33 28 45 ls -1,50 ls +1,50 39 30 38 30 50 ls -1,50 ls +1,50 44 30 43 30 55 ls -1,75 ls +1,75 54 36 48 36 60 ls -1,75 ls +1,75 64 42 63 42 80 ls -1,75 ls +1,75 74 45 73 45 90 ls -2,00 ls +2,00 54 54 54 100 ls -2,00 ls +2,00 70 70 70 120 ls -2,00 ls +2,00 70 70 70 130-300 ls -3,00 ls +3,00 70 70 70 130-300 ls -3,00 ls +3,00 70 70 70 • Screws with partial thread > 60 mm ls with shank ribs 2) Other screw lengths with ls min ≤ ls ≤ ls max and other thread lengths lgf resp. lgp ≥ 4xd up to max. standard thread lengths are allowe									l _s +1,25	5	l _s –1,25	25		
40 $l_s -1,50$ $l_s +1,50$ 34 28 33 28 45 $l_s -1,50$ $l_s +1,50$ 39 30 38 30 50 $l_s -1,50$ $l_s +1,50$ 44 30 43 30 55 $l_s -1,75$ $l_s +1,75$ 49 36 48 36 60 $l_s -1,75$ $l_s +1,75$ 54 36 53 36 70 $l_s -1,75$ $l_s +1,75$ 64 42 63 42 80 $l_s -1,75$ $l_s +1,75$ 74 45 73 45 90 $l_s -2,00$ $l_s +2,00$ 54 54 100 $l_s -2,00$ $l_s +2,00$ 60 60 110 $l_s -2,00$ $l_s +2,00$ 70 70 120 $l_s -2,00$ $l_s +2,00$ 70 70 130-300 $l_s -3,00$ $l_s +3,00$ 70 70 130-300 $l_s -3,00$ $l_s +3,00$ 70 70 310-300 $l_s -3,00$ $l_s +3,00$ 70 70 130-300 $l_s -3,00$ $l_s +3,00$ 70 70 4.11 sizes ²⁾ Other screw lengths with l_s min ≤ $l_s ≤ l_s$ max and other thread lengths l_{gf} resp. $l_{gp} ≥ 4xd$ up to max. standard thread lengths are allowed ³⁾ For 10 mm ≤ l_{gf} resp. $l_{gp} ≤ 18mm →$ tolerance ±1,5 mm and for 18 mm < l_{gf} resp. $l_{gp} ≤ 30 mm →$ tolerance ±1,7 mr						28	24			_			<u> </u>	
50 ls +1,50 44 30 43 30 55 ls -1,75 ls +1,75 49 36 48 36 60 ls -1,75 ls +1,75 54 36 53 36 70 ls -1,75 ls +1,75 64 42 63 42 80 ls -1,75 ls +1,75 74 45 73 45 90 ls -2,00 ls +2,00 54 54 54 100 ls -2,00 ls +2,00 70 70 70 110 ls -2,00 ls +2,00 70 70 70 120 ls -2,00 ls +2,00 70 70 70 130-300 ls -3,00 ls +3,00 70 70 Iscess with partial thread > 60 mm ls with shank ribs 20 Other screw lengths with ls min ≤ ls ≤ ls max and other thread lengths lgr resp. lgp ≥ 4xd up to max. standard thread lengths are allowed 3) For 10 mm ≤ lgr resplgp ≤ 18mm → tolerance ±1,5 mm and for 18 mm < lgr resp. lgp ≤ 30 mm → tolerance ±1,7 mr					28								-	
55 ls -1,75 ls +1,75 49 36 48 36 60 ls -1,75 ls +1,75 54 36 53 36 70 ls -1,75 ls +1,75 64 42 63 42 80 ls -1,75 ls +1,75 74 45 73 45 90 ls -2,00 ls +2,00 54 54 54 100 ls -2,00 ls +2,00 60 60 60 110 ls -2,00 ls +2,00 70 70 70 120 ls -2,00 ls +2,00 70 70 70 130-300 ls -3,00 ls +3,00 70 70 130-300 ls -3,00 ls +3,00 70 70 Issees 2) Other screw lengths with ls min ≤ ls ≤ ls max and other thread lengths lgr resp. lgp ≥ 4xd up to max. standard thread lengths are allowed 3) For 10 mm ≤ lgr resp. lgp ≤ 18mm → tolerance ±1,5 mm and for 18 mm < lgr resp. lgp ≤ 30 mm → tolerance ±1,7 mr					30	38	30	39		_				
60 ls -1,75 ls +1,75 54 36 53 36 70 ls -1,75 ls +1,75 64 42 63 42 80 ls -1,75 ls +1,75 74 45 73 45 90 ls -2,00 ls +2,00 54 54 54 100 ls -2,00 ls +2,00 60 60 60 110 ls -2,00 ls +2,00 70 70 70 120 ls -2,00 ls +2,00 70 70 70 70 130-300 ls -3,00 ls +3,00 70 70 70 70 130-300 ls -3,00 ls +3,00 70 70 70 Issues 2) Other screw lengths with ls min ≤ ls ≤ ls max and other thread lengths lgr resp. lgp ≥ 4xd up to max. standard thread lengths are allowed 3) For 10 mm ≤ lgr resp. lgp ≤ 18mm → tolerance ±1,5 mm and for 18 mm < lgr resp. lgp ≤ 30 mm → tolerance ±1,7 mr										_				
70 $l_s = 1,75$ $l_s + 1,75$ 64 42 63 42 80 $l_s = -1,75$ $l_s + 1,75$ 74 45 73 45 90 $l_s = -2,00$ $l_s + 2,00$ 54 54 100 $l_s = -2,00$ $l_s + 2,00$ 60 60 110 $l_s = -2,00$ $l_s + 2,00$ 70 70 120 $l_s = -2,00$ $l_s + 2,00$ 70 70 130-300 $l_s = -2,00$ $l_s + 2,00$ 70 70 130-300 $l_s = -3,00$ $l_s + 3,00$ 70 70 Issues 2 Other screw lengths with $l_s min \le l_s \le l_s$ max and other thread lengths l_{gf} resp. $l_{gp} \ge 4xd$ up to max. standard thread lengths are allowed 3) For 10 mm $\le l_{gf}$ resp., $l_{gp} \le 18$ mm \rightarrow tolerance $\pm 1,5$ mm and for 18 mm $< l_{gf}$ resp. $l_{gp} \le 30$ mm \rightarrow tolerance $\pm 1,7$ mm										_			⊢	
80 $l_s - 1,75$ $l_s + 1,75$ 74 45 73 45 90 $l_s - 2,00$ $l_s + 2,00$ 54 54 100 $l_s - 2,00$ $l_s + 2,00$ 60 60 110 $l_s - 2,00$ $l_s + 2,00$ 70 70 120 $l_s - 2,00$ $l_s + 2,00$ 70 70 120 $l_s - 2,00$ $l_s + 2,00$ 70 70 130-300 $l_s - 3,00$ $l_s + 3,00$ 70 70 130-300 $l_s - 3,00$ $l_s + 3,00$ 70 70 • Screws with partial thread > 60 mm l_s with shank ribs 2) Other screw lengths with $l_s min \le l_s \le l_s max$ and other thread lengths l_{gf} resp. $l_{gp} \ge 4xd$ up to max. standard thread lengths are allowed 3) For 10 mm ≤ l_{gf} resp., $l_{gp} \le 18$ mm → tolerance ±1,5 mm and for 18 mm < l_{gf} resp. $l_{gp} \le 30$ mm → tolerance ±1,7 mr														
100 $l_s - 2,00$ $l_s + 2,00$ 60 60 110 $l_s - 2,00$ $l_s + 2,00$ 70 70 120 $l_s - 2,00$ $l_s + 2,00$ 70 70 in steps of 10mm											1			
110 $l_s - 2,00$ $l_s + 2,00$ 70 70 120 $l_s - 2,00$ $l_s + 2,00$ 70 70 in steps of 10mm in steps of 10mm in steps of 10mm in steps of 10mm 130-300 $l_s - 3,00$ $l_s + 3,00$ 70 70 • Screws with partial thread > 60 mm l_s with shank ribs 70 70 2) Other screw lengths with $l_s min \le l_s \le l_s$ max and other thread lengths l_{gf} resp. $l_{gp} \ge 4xd$ up to max. standard thread lengths are allowed 3) For 10 mm $\le l_{gf}$ resp. $l_{gp} \le 18$ mm \rightarrow tolerance $\pm 1,5$ mm and for 18 mm $< l_{gf}$ resp. $l_{gp} \le 30$ mm \rightarrow tolerance $\pm 1,7$ mm							-			_				
120 $l_s - 2,00$ $l_s + 2,00$ 70 70 in steps of 10mm - - - - 130-300 $l_s - 3,00$ $l_s + 3,00$ 70 70 All sizes • Screws with partial thread > 60 mm l_s with shank ribs 2) Other screw lengths with $l_s min \le l_s \le l_s max$ and other thread lengths l_{gf} resp. $l_{gp} \ge 4xd$ up to max. standard thread lengths are allowed 3) For 10 mm $\le l_{gf}$ resp. $.l_{gp} \le 18mm \rightarrow$ tolerance $\pm 1,5$ mm and for 18 mm $< l_{gf}$ resp. $l_{gp} \le 30$ mm \rightarrow tolerance $\pm 1,7$ mm										_			-	
in steps of 10mm All sizes 130-300 $l_s -3,00$ $l_s +3,00$ 70 • Screws with partial thread > 60 mm l_s with shank ribs 70 2) Other screw lengths with l_s min $\leq l_s \leq l_s$ max and other thread lengths l_{gf} resp. $l_{gp} \geq 4xd$ up to max. standard thread lengths are allowed 3) For 10 mm $\leq l_{gf}$ resp., $l_{gp} \leq 18$ mm \rightarrow tolerance ±1,5 mm and for 18 mm $< l_{gf}$ resp. $l_{gp} \leq 30$ mm \rightarrow tolerance ±1,7 mm							-						-	
 Screws with partial thread > 60 mm l_s with shank ribs ²⁾ Other screw lengths with l_s min ≤ l_s ≤ l_s max and other thread lengths l_{gf} resp. l_{gp} ≥ 4xd up to max. standard thread lengths are allowed ³⁾ For 10 mm ≤ l_{gf} resp.,l_{gp} ≤ 18mm → tolerance ±1,5 mm and for 18 mm < l_{gf} resp. l_{gp} ≤ 30 mm → tolerance ±1,7 mr 							-		m)mn	eps of 10m	in ste		
 Screws with partial thread > 60 mm l_s with shank ribs ²⁾ Other screw lengths with l_s min ≤ l_s ≤ l_s max and other thread lengths l_{gf} resp. l_{gp} ≥ 4xd up to max. standard thread lengths are allowed ³⁾ For 10 mm ≤ l_{gf} resp.,l_{gp} ≤ 18mm → tolerance ±1,5 mm and for 18 mm < l_{gf} resp. l_{gp} ≤ 30 mm → tolerance ±1,7 mr 		A 11 · · ·			70				l _s +3,00	0	l _s –3,00	0-300	13	
fischer RewerFast II Annex A5	ead	p to max. standard thread			er thread	and othe	l₅ max a	n ≤ l₅ ≤	s with l₅ mi	ths ed	rew length re allowed	Other scr engths a		
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Table A6: Screw sizes and material

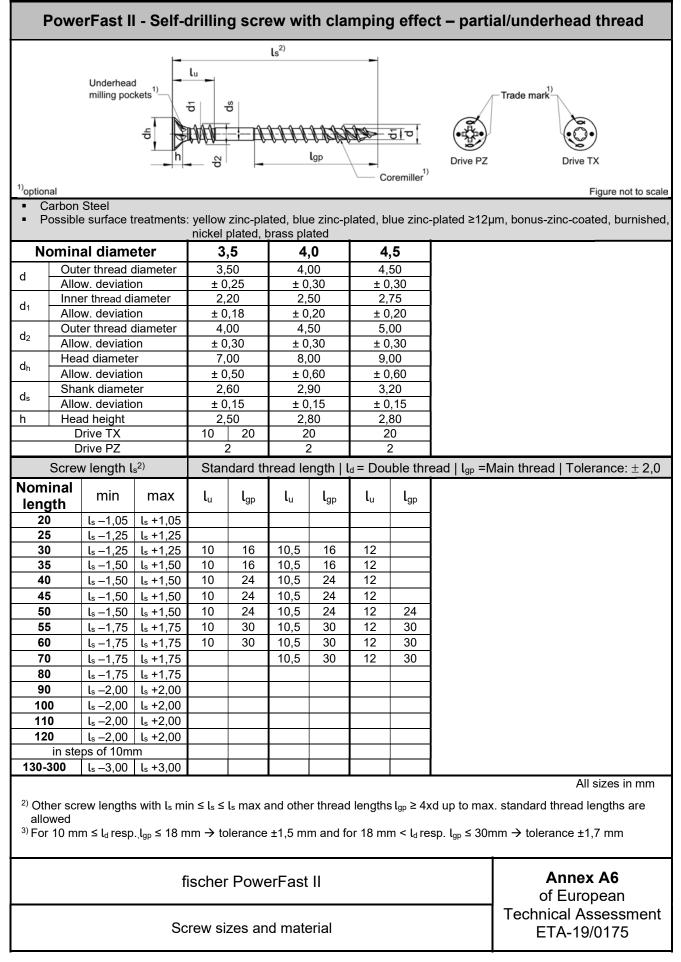




Table A7: FAFS-Clip size and material

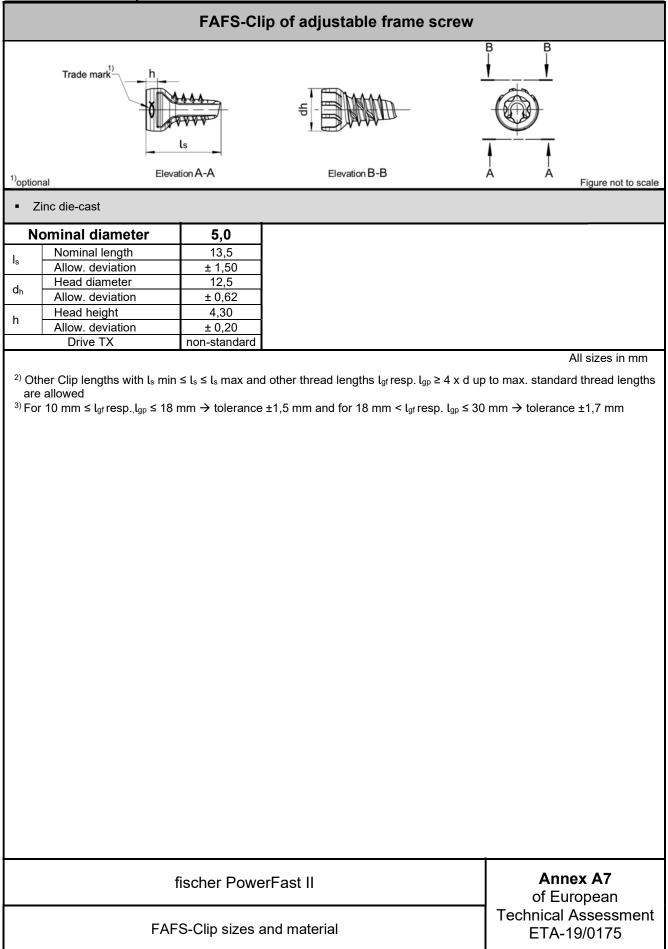
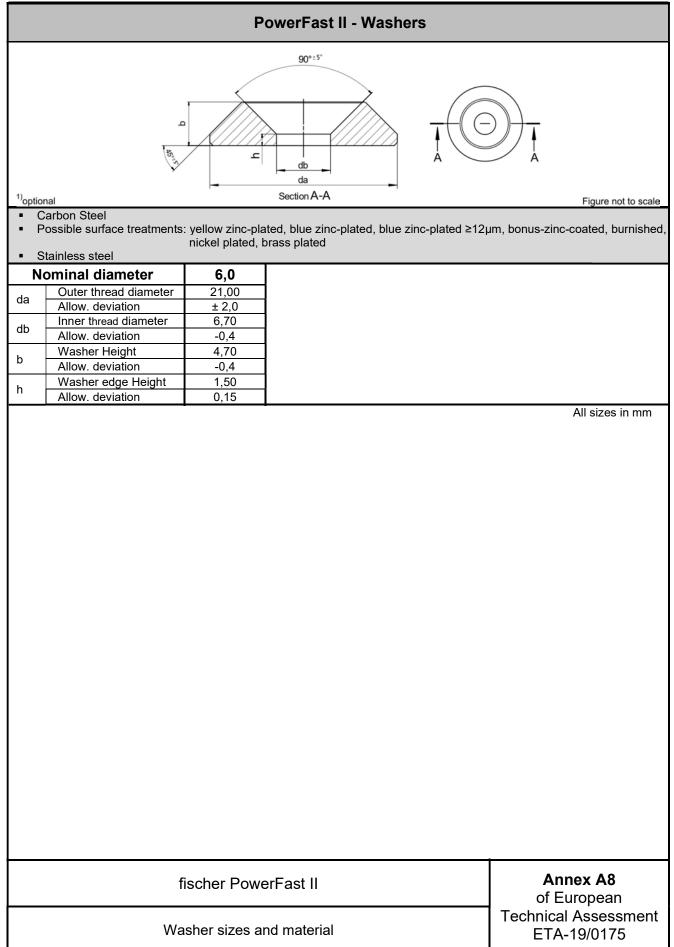


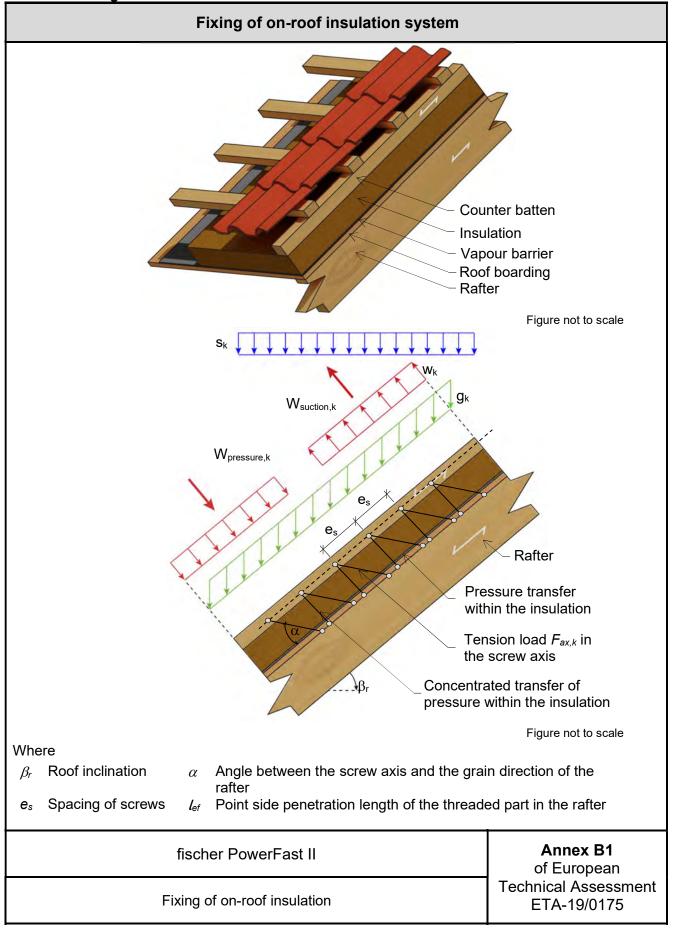


Table A8: Washer sizes and material

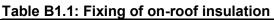












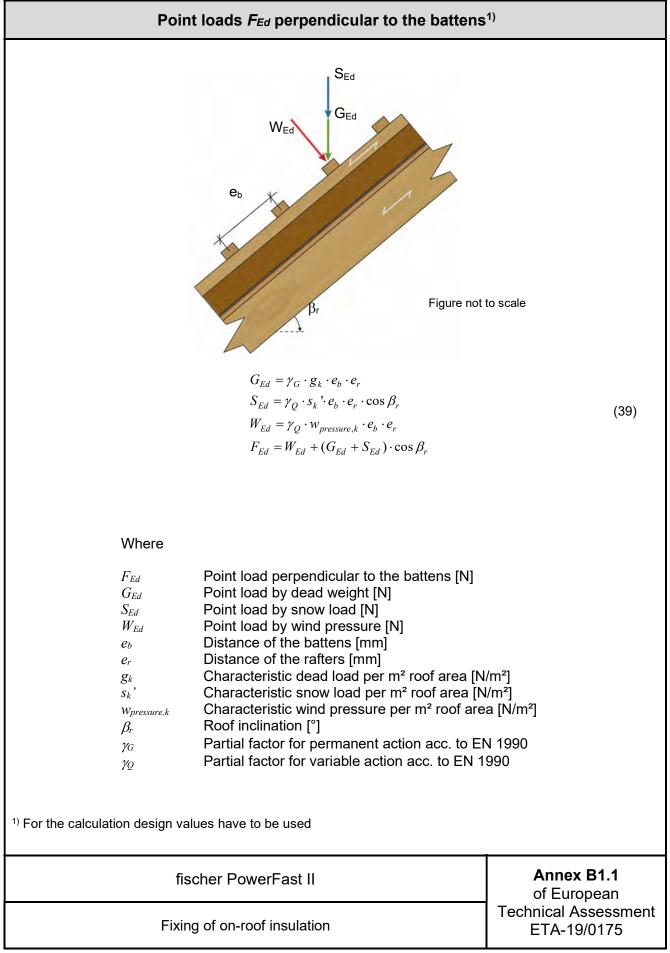




Table B1.2: Fixing of on-roof insulation

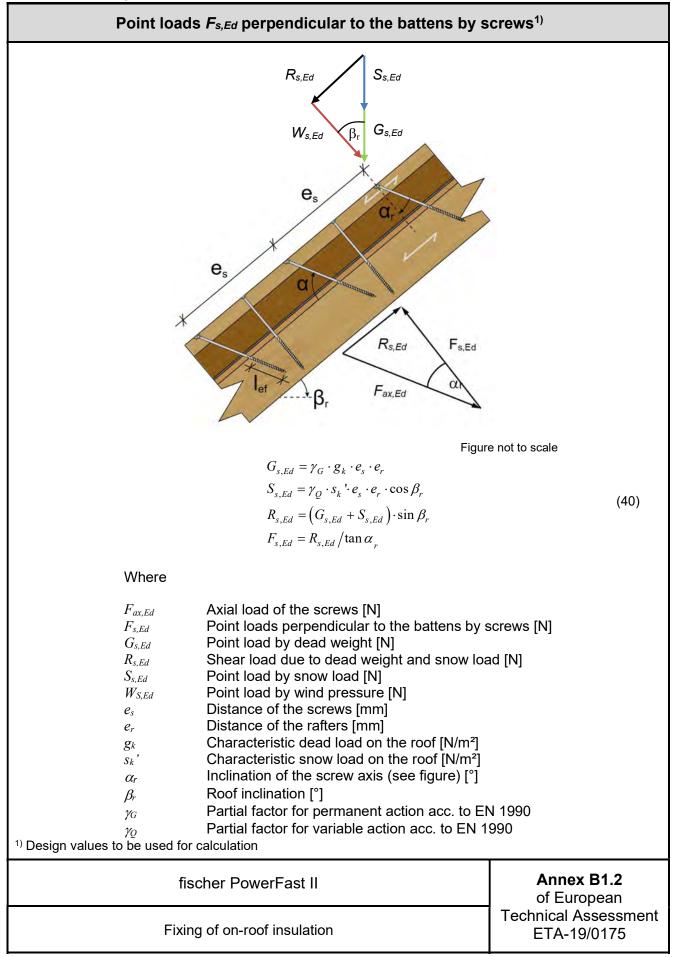




Table B1.3: Fixing of on-roof insulation

	Design of the battens	
The bending	stresses of the battens are calculated with	
	$M_{Ed} = \frac{\left(F_{Ed} + F_{s,Ed}\right) \cdot l_{char}}{4}$	(41)
Where		
F _{Ed} F _{s,Ed} M _{Ed} I _{char}	Point loads perpendicular to the battens [N] Point loads perpendicular to the battens in the area of the set Design bending moment of the batten [Nmm] Characteristic length of the batten [mm] with $l_{char} = \sqrt[4]{\frac{4 \cdot EI}{w_{ef} \cdot K}}$, where EI Bending stiffness of the batten [Nmm ²] w_{ef} Effective width of the thermal insulation [mm] with $w_{ef} = w + t_{ti} / 2$, where w Minimum width of the batten or rafter [mm] t_{ti} Thickness of the thermal insulation [mm] K Bedding modulus [N/mm ³]	rew heads [N]
	The coefficient \vec{k} may be calculated from the mo- the thickness t_{ti} of the thermal insulation if the effective thermal insulation under compression is known. In extension in the insulation the effective width w_{ef} of the batten or rafter, respectively. For further ca	ective width w_{ef} of the Due to the load is greater than the width alculations, the effective
	width w_{ef} of the thermal insulation may be determ	ined with $K = \frac{E_{ti}}{t_{ti}}$, where
The following	E_{ti} Modulus of elasticity of the thermal insulation t_{ti} Thickness of the thermal insulation [mm] g conditions shall be satisfied:	" [N/mm²]
	-	(42)
	$\frac{\sigma_{m,Ed}}{f_{m,d}} \leq 1$	(42)
Where		
$\sigma_{m,Ed}$ f _{m,d}	Design value of the bending stress of the batten [N/mm²] Design value of the bending strength [N/mm²]	
	$\frac{\tau_{Ed}}{f_{v,d}} = \frac{3 \cdot V_{Ed}}{2 \cdot A_{ef} \cdot f_{v,d}} \le 1$	(43)
Where $f_{v,d}$ A_{ef} V_{Ed}	Design value of the shear strength of the batten [N/mm ²] Net cross section of the batten [mm ²] Design shear load onto the batten [N] with $V_{Ed} = \frac{F_{Ed} + F_{s,Ed}}{2}$	
$ au_{Ed}$	Design value of the shear stress of the batten [N/mm ²]	
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	Fixing of on-roof insulation	Technical Assessment ETA-19/0175



Table B1.4: Fixing of on-roof insulation

Design of the heat insulation

The compressive stresses in the thermal insulation shall be calculated with $\sigma_{c,Ed} = \frac{1.5 \cdot F_{Ed} + F_{s,Ed}}{2 \cdot l_{char} \cdot w_{ef}}$ (44) Where Point loads perpendicular to the battens [N] F_{Ed} Point loads perpendicular to the battens in the area of the screw heads [N] $F_{s,Ed}$ Characteristic length of the batten [mm] lchar with $l_{char} = \sqrt[4]{\frac{4 \cdot EI}{w_{of} \cdot K}}$, where Bending stiffness of the batten [Nmm²] EIWef Effective width of the thermal insulation [mm] with $w_{ef} = w + t_{ti} / 2$, where w Minimum width of the batten or rafter [mm] t_{ti} Thickness of the thermal insulation [mm] Κ Bedding modulus [N/mm³] The coefficient K may be calculated from the modulus of elasticity E_{ti} and the thickness t_{ii} of the thermal insulation if the effective width w_{ef} of the thermal insulation under compression is known. Due to the load extension in the insulation the effective width w_{ef} is greater than the width of the batten or rafter, respectively. For further calculations, the effective width w_{ef} of the thermal insulation may be determined with $K = \frac{E_{ti}}{K}$, where E_{ti} Modulus of elasticity of the thermal insulation [N/mm²] t_{ti} Thickness of the thermal insulation [mm] Design value of the compression stresses of the thermal insulation $\sigma_{c,Ed}$ Note: The design value of the compressive stress shall not be greater than 110 % of the compressive stress at 10 % deformation calculated according to EN 826. Annex B1.4 fischer PowerFast II of European **Technical Assessment** Fixing of on-roof insulation ETA-19/0175



Table B1.5: Fixing of on-roof insulation

Design of the screws

The screws are loaded predominantly axially. The axial tension force in the screw may be calculated from the shear loads of the roof

$$F_{ax,Ed} = \frac{R_{s,Ed}}{\cos \alpha_r} \le F_{ax,\alpha,Rd}$$
(45)

Where

$F_{ax,Ed}$	Design value of the axial tension forces onto the screw [N]
$F_{ax, \alpha, Rd}$	Design value of the withdrawal capacity of the screw [N]
$R_{s,Ed}$	Shear loads onto the screw [N]
α_r	Angle inclined screw (see figure B1.2) [°]

The load-carrying capacity of axially loaded screws is the minimum design value of the axial withdrawal capacity of the threaded part of the screw, the head pull-through capacity of the screw and the tensile capacity of the screw.

In order to limit the deformation of the screw head for heat insulation thicknesses over 200 mm or with compressive strength below 0,12 N/mm², respectively, the axial withdrawal capacity of the screws shall be reduced by the factors k_1 and k_2 .

$$F_{ax,\alpha,Rd} = \min\left\{k_{ax} \cdot f_{ax,d} \cdot d \cdot l_{ef} \cdot k_1 \cdot k_2 \cdot \left(\frac{\rho_k}{350}\right)^{0,8}, f_{head,d} \cdot d_h^2 \cdot \left(\frac{\rho_k}{350}\right)^{0,8}, f_{tens,d}\right\}$$
(46)

Where

F	Design value of the withdrawal capacity of the screw [N]				
$F_{ax, \alpha, Rd}$					
d	Diameter of the screw [mm]				
d_h	Head diameter of the screw [mm]				
$f_{ax,d}$	Design value of the withdrawal parameter of the threaded part of the screw				
	[N/mm ²]				
$f_{head,d}$	Design value of the head pull-through capacity of the screw [N/mm ²]				
$f_{tens,d}$	Design value of the tensile capacity of the screw [N]				
<i>k</i> _{ax}	Coefficient according to equation (11)				
k_1	$min \{1; 200 / t_{ij}\}$ [-]				
k_2	min {1; $\sigma_{10\%,Ed}$ / 0,12} [-], where				
	$\sigma_{10\%Ed}$ Compressive stress of the heat insulation at 10 % deformation				
	[N/mm ²]				
	<i>t_{ti}</i> Thickness of the thermal insulation [mm]				
l _{ef}	Point side penetration length of the threaded part in the rafter with $l_{ef} \ge 40$ mm				
α	Angle between grain and screw axis ($\alpha > 30^\circ$) [°]				
$ ho_k$	Characteristic density of the timber element [kg/m ³]				
PK					

Note: If in the equation for $F_{ax,Rd}$ the factors k_1 and k_2 are considered, the deflection of the battens does not need to be considered. Alternatively to the battens, panels with a minimum thickness of 20 mm from plywood according to EN 636 or an ETA or national provisions that apply at the installation site, particle board according to EN 312 or an ETA or national provisions that apply at the installation site, oriented strand board according to EN 300 or an ETA or national provisions that apply at the installation site and solid wood panels according to EN 13353 or an ETA or national provisions that apply at the installation site or Cross- laminated Timber according to an ETA may be used.

> fischer PowerFast II Fixing of on-roof insulation

Annex B1.5 of European Technical Assessment ETA-19/0175



Table B1.6: Fixing of on-roof insulation

Thermal insulation material on rafters with parallel screws perpendicular to the roof plane

Alternative to the battens, panels with a minimum thickness of 20 mm from plywood according to EN 636, particleboard according to EN 312, oriented strand board OSB/3 and OSB/4 according to EN 300 or European Technical Assessment and solid wood panels according to EN 13353 may be used.

Characteristic load-carrying capacity of a screw loaded in shear:

$$F_{v,Rk} = min \begin{cases} f_{h,b,k} \cdot d \cdot t_{b} \\ f_{h,r,k} \cdot d \cdot t_{r} \\ \frac{f_{h,b,k} \cdot d \cdot \beta}{1+\beta} \cdot \left(\sqrt{4t_{ti}^{2} + (2+\frac{1}{\beta})t_{b}^{2} + (2+\beta)t_{r}^{2} + 4t_{ti}\left(t_{b} + t_{r}\right) + 2t_{b}t_{r}} - 2t_{ti} - t_{b} - t_{r}\right) + \frac{F_{ax,Rk}}{4} \\ 1,05 \cdot \frac{f_{h,b,k} \cdot d \cdot \beta}{\frac{1}{2} + \beta} \left(\sqrt{t_{ti}^{2} + t_{ti}t_{b} + \frac{t_{b}^{2}}{2}\left(1 + \frac{1}{\beta}\right) + \frac{M_{y,k}}{f_{h,b,k} \cdot d}\left(1 + \frac{2}{\beta}\right)} - t_{ti} - \frac{t_{b}}{2}\right) + \frac{F_{ax,Rk}}{4} \\ 1,05 \cdot \frac{f_{h,b,k} \cdot d \cdot \beta}{\frac{1}{2} + \beta} \left(\sqrt{t_{ti}^{2} + t_{ti}t_{r} + \frac{t_{r}^{2}}{2}\left(1 + \beta\right) + \frac{M_{y,k}}{f_{h,b,k} \cdot d}\left(2 + \frac{1}{\beta}\right)} - t_{ti} - \frac{t_{r}}{2}\right) + \frac{F_{ax,Rk}}{4} \\ 1,05 \cdot \frac{f_{h,b,k} \cdot d \cdot \beta}{\frac{1}{2} + \beta} \left(\sqrt{t_{ti}^{2} + t_{ti}t_{r} + \frac{t_{r}^{2}}{2}\left(1 + \beta\right) + \frac{M_{y,k}}{f_{h,b,k} \cdot d}\left(2 + \frac{1}{\beta}\right)} - t_{ti} - \frac{t_{r}}{2}\right) + \frac{F_{ax,Rk}}{4} \\ 1,15 \cdot \frac{f_{h,b,k} \cdot d}{1 + \beta} \left(\sqrt{\beta^{2}t_{ti}^{2} + 4 \cdot \beta(\beta + 1) \cdot \frac{M_{y,k}}{f_{h,b,k} \cdot d}} - \beta \cdot t_{ti}\right) + \frac{F_{ax,Rk}}{4} \end{cases}$$

Where

$F_{ax,Rk}$ The minimum characteristic load-carrying capacity of the axially loaded screws acc. to EN 1995-1-1 [N] $f_{h,h,k}$ Characteristic embedment strength of the batten [N/mm²] $f_{h,r,k}$ Characteristic embedment strength of the rafter [N/mm²] d Outer thread diameter [mm] t_b Batten thickness [mm] t_r The lower value of rafter thickness or screw penetration length [mm] t_i Thickness of the thermal insulation [mm] β Coefficient of the embedment strength of the rafter to the batten [-] with $\beta = \frac{f_{h,r,k}}{f_{h,b,k}}$ fischer PowerFast II Annex B1.6 of European
screws acc. to EN 1995-1-1 [N] $f_{h,b,k}$ Characteristic embedment strength of the batten [N/mm²] $f_{h,r,k}$ Characteristic embedment strength of the rafter [N/mm²] d Outer thread diameter [mm] t_b Batten thickness [mm] t_r The lower value of rafter thickness or screw penetration length [mm] t_{ii} Thickness of the thermal insulation [mm] β Coefficient of the embedment strength of the rafter to the batten [-]
$F_{v,RK}$ Characteristic load-carrying capacity of a screw loaded in shear [N] $M_{y,k}$ Characteristic yield moment of the screw [Nmm]



Table B2: FAFS-Clip

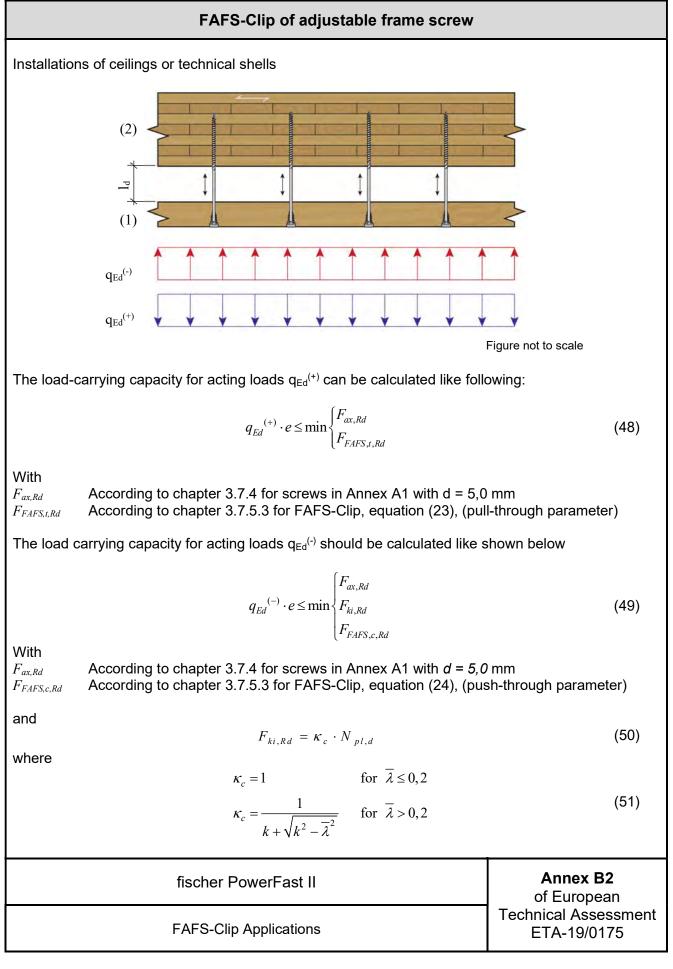




Table B2.1: FAFS-Clip

FAFS-Clip of adjustable frame screw

with

$$k = 0, 5 \cdot \left[1 + 0, 49 \cdot \left(\overline{\lambda} - 0, 2\right) + \overline{\lambda}^2\right]$$
(52)

The relative slenderness ratio shall be calculated with

$$\overline{\lambda} = \frac{4 \cdot L_{cr}}{\pi \cdot (0, 7 \cdot d)} \cdot \sqrt{\frac{f_{y,k}}{E_s}}$$
(53)

With the characteristic value for the axial capacity in case of plastic analysis referred to the diameter

$$N_{pl,k} = \frac{(0,7 \cdot d)^2 \cdot \pi}{4} \cdot f_{y,k}$$
(54)

For screws with a diameter of 5 mm, according to Annex A1

$$N_{pl,k} = 8710 \text{ N}$$
 (55)

And the buckling length L_{cr} on the side of the screw tip with a minimum penetration depth of $8 \cdot d$

$$L_{cr} = 0, 7 \cdot l_d \tag{56}$$

Where

d e Es	Nominal diameter of the screw [mm] Effective distance (supporting points) between parallel arranged screws [m] Modulus of elasticity of the screw [N/mm²], see chapter 3.7.7
$F_{ax,Rd}$	Design withdrawal capacity of the screw in the structural timber element (2) [N], see chapter 3.7.4
$F_{FAFS,t,Rd}$	Design head pull-through capacity of the FAFS-Clip in timber part (1) for tension forces [N], see chapter 3.7.5.3
$F_{FAFS,c,Rd}$	Design head push-through capacity of the FAFS-Clip in timber part (1) for compression forces [N], see chapter 3.7.5.3
L_{cr}	Buckling length of the screw [mm]
l_d	Distance between (1) and (2) [mm]
$N_{pl,k}$	Characteristic axial capacity in case of plastic analysis [N]
$q_{Ed}^{(+)}$	Design load effecting tension loads on the installation element (1) [N/m]
$q_{Ed}^{(-)}$	Design load effecting compression loads on the installation element (1) [N/m]

Note: The compressive capacity must be modified for $f_{ax,d}$ with the factors k_{mod} and γ_M for timber according to EN 1995-1-1 while $N_{pl,d}$ the partial-factor $\gamma_{M,1}$ for steel buckling according to EN 1993-1-1 and/or national standards must be considered.

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FAFS-Clip Applications

Annex B2.1 of European Technical Assessment ETA-19/0175



Table B3: Inclined Screws

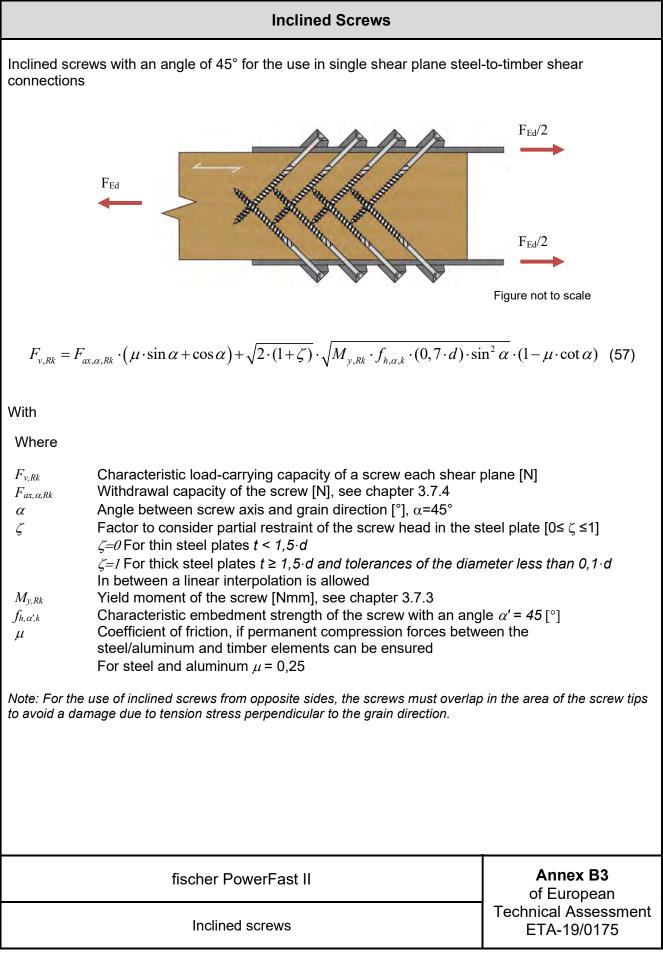




Table B3.1: Inclined Screws

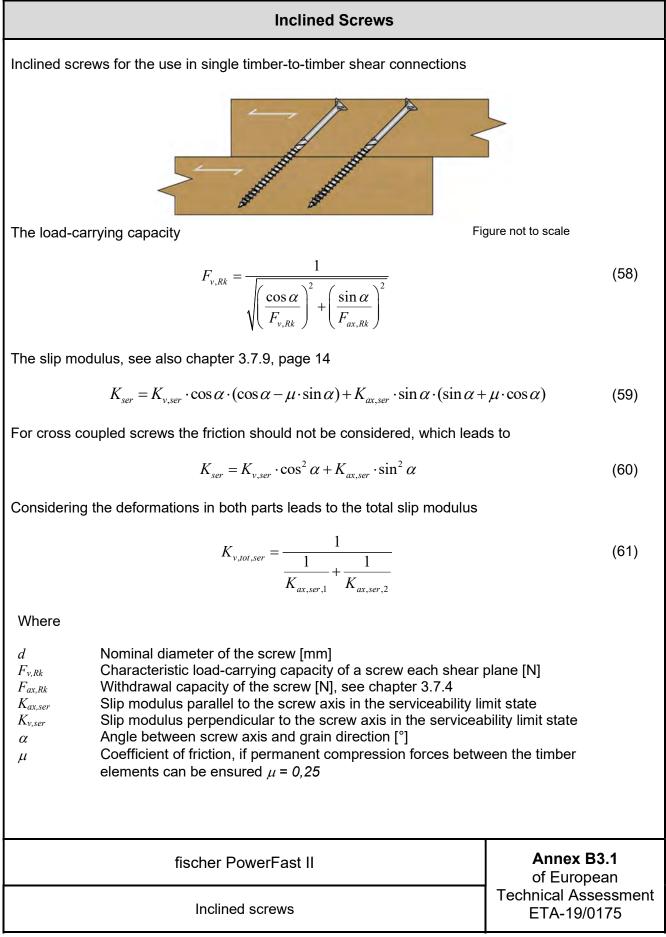
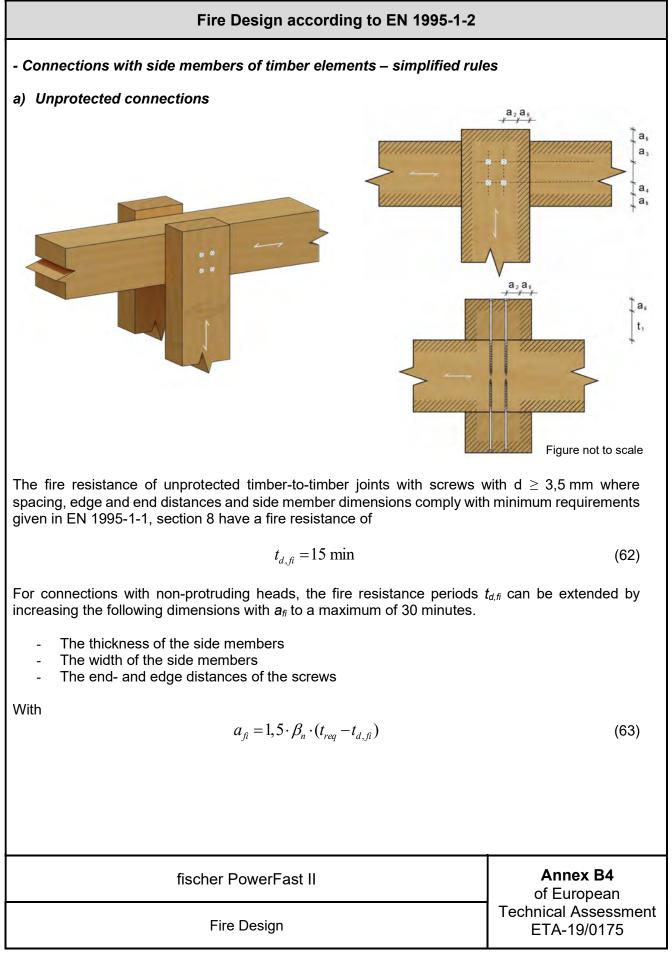




Table B4: Fire Design





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Table B4.1: Fire Design

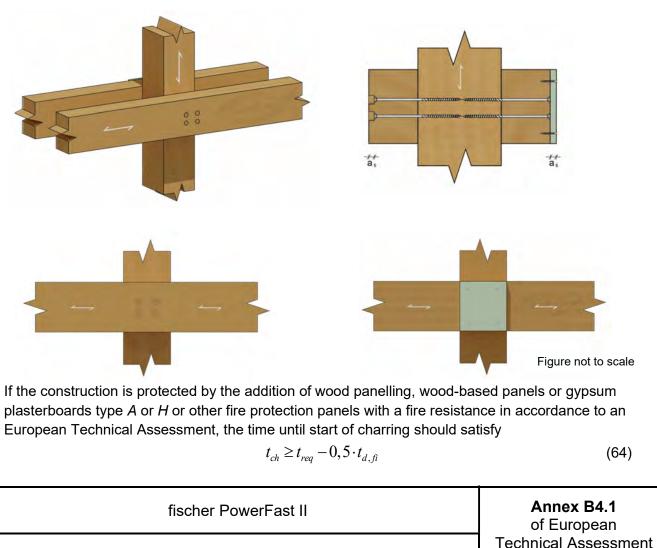
Fire Design according to EN 1995-1-2

The values for the design notional charring rate β_n under standard fire exposure are given below.

Table B4.1: Notional charring rate

Material	β _n [mm/min]
Softwood and beech	
Glued-Laminated Timber with a characteristic density of \geq 290 kg/m ³	0,70
Solid Timber with a characteristic density of \geq 290 kg/m ³	0,80
Hardwood	
Solid or Glued-Laminated hardwood with a characteristic density of \geq 290 kg/m ³	0,70
Solid or Glued-Laminated hardwood with a characteristic density of \ge 450 kg/m ³	0,55
LVL	
LVL with a characteristic density of \geq 480 kg/m ³	0,70

b) Protected connections



Fire Design

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Table B4.2: Fire Design

Fire Design according to EN 1995-1-2

If the connection is protected by the addition of gypsum plasterboard type F, the time until start of charring should satisfy equation (65).

$$t_{ch} \ge t_{req} - 1, 2 \cdot t_{d,fi} \tag{65}$$

For connections where the screws are protected by glued-in timber plugs, the length of the plugs should be determined according to

$$a_{fi} = 1, 5 \cdot \beta_n \cdot (t_{reg} - t_{d,fi})$$
(66)

The fixings of the additional protection should prevent its premature failure. Additional protection provided by wood-based panels or gypsum plasterboards should remain in place until charring of the member starts ($t = t_{ch}$). Additional protection provided by gypsum plasterboards type *F* should remain in place during the required fire resistance period ($t = t_{req}$).

The following rules apply for the fixing of additional protections by screws:

- The distance between the screws should be not more than 100 mm along the board edges and not more than 300 mm for fastenings within the area of the boards
- The edge distance of fasteners should be equal or greater than *a*_{fi}, calculated using expression

$$a_{fi} = 1, 5 \cdot \beta_n \cdot (t_{reg} - t_{d,fi}) \tag{67}$$

The penetration depth of the screws for fixing the additional protection made of wood, woodbased panels or gypsum plasterboards type A or H should be at least $6 \cdot d$.

For gypsum plasterboards type F, the penetration length into unburnt wood (that is beyond the char-line) should be at least 10 mm (see also EN 1995-1-2).

Where

- a_{fi} Extra thickness of member to improve the fire resistance [mm]
- *t_{req}* Required time of fire resistance [min]
- $t_{d,fi}$ Time of the fire resistance of the unprotected connection [min]

 β_n Notional charring rate [mm/min]

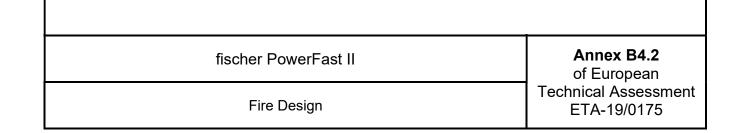
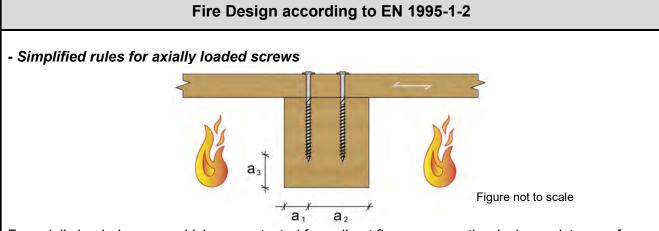




Table B4.3: Fire Design



For axially loaded screws which are protected from direct fire exposure, the design resistance of the screws should be calculated like below

$$F_{ax,d,t,fi} = \eta \cdot \frac{1,05 \cdot F_{ax,Rk}}{\gamma_{M,fi}}$$
(68)

For connections where the distances a_2 and a_3 of the screws satisfy the equations (69), the conversion factor η for the reduction of the axial resistance of the screw in the fire situation should be calculated with equation (70).

$$a_2 \ge a_1 + 40$$

 $a_3 \ge a_1 + 20$ (69)

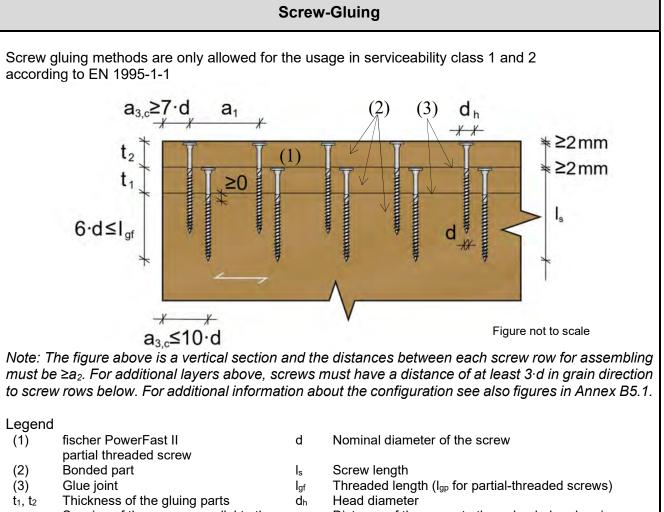
$$\eta = \begin{cases} 0 & \text{for } \mathbf{a}_{1} \leq 0, 6 \cdot t_{d,fi} \\ \frac{0, 44 \cdot a_{1} - 0, 264 \cdot t_{d,fi}}{0, 2 \cdot t_{d,fi} + 5} & \text{for } 0, 6 \cdot t_{d,fi} \leq \mathbf{a}_{1} \leq 0, 8 \cdot t_{d,fi} + 5 \\ \frac{0, 56 \cdot a_{1} - 0, 36 \cdot t_{d,fi} + 7, 32}{0, 2 \cdot t_{d,fi} + 23} & \text{for } 0, 8 \cdot t_{d,fi} + 5 \leq \mathbf{a}_{1} \leq t_{d,fi} + 28 \\ 1, 0 & \text{for } \mathbf{a}_{1} \geq t_{d,fi} + 28 \end{cases}$$
(70)

Where

a ₁ , a ₂ , a ₃ t _{d,fi} F _{ax,Rk} F _{ax,d,t,fi} γ _{M,fi}	Distances and spacing of the screws [mm] Time of the fire resistance of the unprotected connection [mi Characteristic withdrawal strength [N] Design value of the withdrawal strength in the fire situation [Partial factor for timber in the case of fire, see National regul (recommended value $\gamma_{M,fire}$ =1,0) [-] Conversion factor for the reduction of the load-bearing capa- case of fire [-]	N] lations		
	fischer PowerFast II	Annex B4.3 of European		
Fire DesignTechnical AssesETA-19/017				



Table B5: Screw-Gluing



a1 Spacing of the screws parallel to the grain in a row

a_{3,c} Distance of the screw to the unloaded end grain

The shown applications for screw-bonding applies only for structures in serviceability class 1 and 2 according to EN 1995-1-1. The use of an adhesive with joint filling properties is necessary. If the joint thickness of a maximum of 0,3 mm can be ensured, adhesives according to EN 15425 and adhesives type I may also be used according to EN 301. The adhesive manufacturer's instructions must be fulfilled. Only »fischer PowerFast II« screws with washer or step countersunk heads (see Annex A4 and A5) with a nominal diameter $d \ge 5$ mm should be used.

In the use of partial-threaded screws, no part of the thread should be in the bonded part. When using fully threaded screws, the glued part must be pre-drilled with a borehole of at least d + 1,0 mm. The upper side of the screw head or the washer, must be countersunk at least 2 mm from the surface of the glued part. The figure above shows the different options for installing the partial threaded screws of the assembling structural elements.

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Screw -Gluing

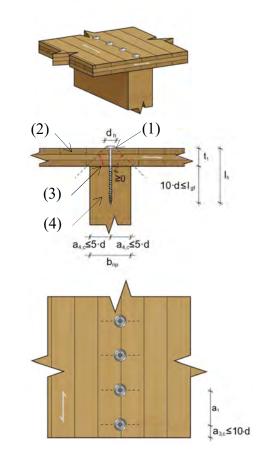
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Table B5.1: Screw-Gluing

Screw-Gluing

The minimum spacing for connections with axially loaded screws must be observed. The maximum distance in the adhesive surface to the ends of the components must be $a_{3,c} \le 10 \cdot d$, and to the edges $a_{4,c} \le 5 \cdot d$. With a single-row screw connection, the rib width b_{rib} may not be larger than $d_h + 2 \cdot t_1$, otherwise a multi-row screw connection must be carried out.



Legend

- (1) Partial threaded screw with washer
- (3) Glue joint
- a_1 Spacing of the screws parallel to the a_1^* grain in a row
- a_2 Spacing of the screws perpendicular
to the grain direction $a_{3,c}$ $a_{4,c}$ Distance to the unloaded edge b_{rip}
- $a_{4,c}$ Distance to the unloaded edgedNominal diameter of the screw
- *I*_s Screw length
- t_1 Thickness of the bonded panel



(4) Rib (timber beam)

a3c≥7.d

Reduced spacing of the screw parallel to the grain in a row to ensure a distance of a₁/2 between adjoining screw rows

a₄ ≤5 ·d

a

brip

0

00

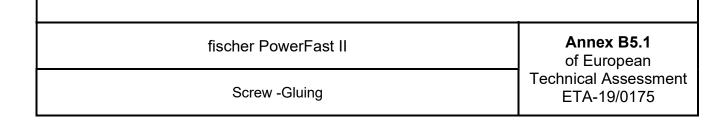
10·d≤

a_{3,c}≤10·d

Figure not to scale

a₄ ≤5·d

- Distance to the unloaded end grain
- Width of the beam web
- Head diameter
- Threaded length (l_{gp} for partial-threaded screws)



dh

lgf



Table B5.2: Screw-Gluing

Screw-Gluing

The surfaces of the bonded parts must be suitable for bonding and are in accordance to the requirements of the adhesive manufacturer. In general, the finishes need be sanded or smoothed planed and without coatings, dirt, dust and impurities.

The tolerance of the joint thickness of the assembling parts must fulfil the tolerances for

- Beam- and plate-shaped screw-gluing: max. 1 mm per 1 m
- Ribbed panels: max. 2 mm per 2 m

If several layers are glued together, each layer must be screwed-on separately. The screws must be arranged staggered (see also figure Annex B 5.1, right below), to apply enough pressure in all joints. In the intermediate layers, the screw heads should not protrude the surface of the intermediate layer.

Deformations and movements that lead to damages of the adhesive-joints have to be avoided. The screw parameters and distances depend on the thickness of the assembling parts, given in the table below.

Material bonded part	Thickness bonded part	Recommended nominal diameter	Min. nominal head diameter	Maximum scree Parallel to the grain direction of the outer layer	Perpendicu to the grai direction of outer laye	n screw part the in the r structural part	Calculated compressive stress <i>p</i> _{cal,min}
Beem and nenel abo	[mm]	[mm]	[mm]	[mm]	[mm]	[mm]	[N/mm²]
Beam- and panel sha LVL of softwood, three-layered solid timber panel, OSB	$12 \le t < 19$	<i>g</i> ≥ 5 e.g Annex A4, A5	9,8	100	65	6·d	
LVL beech		Annex A 1 , A0		100	100	8·d	
Lamellas and one- layered solid timber panels		≥ 6	10,8	140	65	6∙d	0,10
LVL in spruce three-layered solid timber panel, OSB	19 ≤ t < 27	e.g Annex A1	Washer, e.g Annex A8	140	90	6∙d	
LVL beech			10,8	140	140	8·d	
fischer PowerFast II				т	Annex B5.2 of European Technical Assessment		
Screw -Gluing E				ETA-19/0	0175		

Table B5.2: Properties of the bonded parts, screw parameters and compressive stress



Table B5.3: Screw-Gluing

Screw-Gluing

As an alternative to the specifications in the table Annex B5.2, the maximum screw spacing can also be determined with the empirical equation (71).

$$a_{i,max} = 3,35 \cdot \sqrt[4]{E_{mean,i} \cdot I_{i,b=1}}$$
(71)

with *i* = 1 or 2

In addition, it must be proven that the calculated minimum compressive stress per screw is observed

$$\frac{F_{ax,Rd}}{a_1 \cdot a_2} \ge p_{cal,min} \tag{72}$$

Where

$a_{i,max}$	Maximum spacing of the screws in i-direction [mm]
$I_{i.b=1}$	Moment of inertia in i-direction for a width of 1 mm of the bonded part [mm ⁴]
$E_{mean,i}$	Modulus of elasticity in i-direction of the bonded part [N/mm ²]
$a_{i,max}$	Maximum spacing of the screws [mm]
$F_{ax,Rd}$	Design withdrawal strength of the screw [N]
$p_{cal,min}$	Minimum calculated compressive stress according to Annex B5.2

For the characteristic head pull-through parameter $f_{head,k}$ the following models can be used:

- Screws with glued parts made of solid timber and wood-based materials in softwood with

$$f_{head,k} = 14 \cdot d_h^{-0.14} \cdot \left(\frac{\rho_k}{\rho_a}\right)^{0.8}$$
(73)

- Screws with glued parts made of LVL in beech with

$$f_{head,k} = 25 \text{ N/mm}^2 \tag{74}$$

The decrease in the pressure until the adhesive hardens, can be taken into account in the calculation model with $k_{mod} = 1,0$ and $\gamma_M = 1,3$. Table in Annex B5.2 is based on these model assumptions. After the required bond strength has been reached, the screws can be unscrewed.

